Full Download: https://testbanklive.com/download/introduction-to-hydrology-5th-edition-viessman-solutions-manual/

# Solutions Manual

# INTRODUCTION TO HYDROLOGY FIFTH EDITION

Warren Viessman, Jr. University of Florida

Gary L. Lewis Consulting Engineer



Pearson Education, Inc. Upper Saddle River, New Jersey 07458 Acquisitions Editor: Laura Fischer Supplement Editor: Erin Katchmar

Executive Managing Editor: Vince O'Brien

Managing Editor: David A. George Production Editor: Barbara A. Till

Supplement Cover Manager: Daniel Sandin

Manufacturing Buyer: Ilene Kahn



© 2003, 1996, 1989, 1977, 1972 by Pearson Education, Inc. Pearson Education, Inc. Upper Saddle River, NJ 07458

All rights reserved. No part of this book may be reproduced in any form or by any means, without permission in writing from the publisher.

The author and publisher of this book have used their best efforts in preparing this book. These efforts include the development, research, and testing of the theories and programs to determine their effectiveness. The author and publisher make no warranty of any kind, expressed or implied, with regard to these programs or the documentation contained in this book. The author and publisher shall not be liable in any event for incidental or consequential damages in connection with, or arising out of, the furnishing, performance, or use of these programs.

Printed in the United States of America

10 9 8 7 6 5 4 3 2 1

#### ISBN 0-13-008100-0

Pearson Education Ltd., London

Pearson Education Australia Pty. Ltd., Sydney

Pearson Education Singapore, Pte. Ltd.

Pearson Education North Asia Ltd., Hong Kong

Pearson Education Canada, Inc., Toronto

Pearson Educación de Mexico, S.A. de C.V.

Pearson Education—Japan, Tokyo

Pearson Education Malaysia, Pte. Ltd.

Pearson Education, Inc., Upper Saddle River, New Jersey

# Contents

| 1  | Introduction                                   | 1   |
|----|--|-----|
| 2  | Hydrologic Measurements and Data Sources       | 2   |
| 3  | Statistical Methods in Hydrology               | 3   |
| 4  | Precipitation                                  | 26  |
| 5  | Interception and Depression Storage            | 33  |
| 6  | Evaporation and Transpiration                  | 34  |
| 7  | Infiltration                                   | 37  |
| 8  | Surface Water Hydrology                        | 42  |
| 9  | Hydrographs                                    | 46  |
| 10 | Groundwater Hydrology                          | 92  |
| 11 | Urban Hydrology                                | 103 |
| 12 | Hydrologic Simulation and Streamflow Synthesis | 109 |
| 13 | Hydrology in Design                            | 126 |

#### CHAPTER 1

 $100*10^6*0.02 = 2*10^6 \text{ m}^3$ 1.1 1 acre-ft = 43.560 cubic feet cubic meters\*35.31 = cubic feet  $(2*10^6*35.31)/43,560 = 1,612.2$  acre-ft 1.2 volume/volume per unit time = time (500,000\*0.3)/(0.5) = 300,000 sec.300,000/3,600 = 83.3 hours 1.3 (450 + 500)/2 - (500 + 530)/2 = avg. inflow - avg. outflowthe change in storage is thus - 40 cfs -40\*3600/43560 = -3.31, the change in storage in acre-ft. The initial storage is thus depleted by 3.31 ac-ft 3.31\*43,560/35.31 = 4,083 cubic meters 1.4 125/365 = 0.34 cm/day = 0.035 cm/day0.34/2.54 = 0.13 in./day 1.5 volume = 5280\*5280\*0.5 = 13,939,220 cubic feet V/O = time13,939,220\*3600/12 = 1,161,600 sec, or 322.7 hr, or 13.4 days1.6 ET = P - R $R = (140*3600*24*365)/(10,.000*1000^2) =$ 0.44 m/yr or 44 cm/yr ET = 105 - 44 = 61 cm/yrThis is a crude estimate. equivalent depth = vol/area 1.7 inflow = 25\*3600\*24\*365 = 788,400 cubic feet/yrinflow/(3650\*43560) = 4.96 ft/yrE = 100\*365/3650 = 10.0 ft/yrHence there is a drop in level of 5.04 ft

Iavg. - Oavg. = change in storage per unit time

The storage is thus increased by 7,200 cubic meters resulting in a final storage of 27,200 cubic meters

(20 - 18)\*3600 = 7,200 cubic meters

1.8

# **CHAPTER 2**

Problems in this chapter are to be developed by the instructor.

## **CHAPTER 3**

- 3.1 3.4 To be assigned by instructor.
- 3.5 For the James River rainfall:

| Interval in. | $\underline{\mathbf{f}}$ | $\underline{\Sigma \mathbf{f}}$ | $\underline{P(x)}$ | F(x)        |
|--------------|--------------------------|---------------------------------|--------------------|-------------|
| (36-37)      | 2                        | 2                               | 0.057              | 0.057       |
| (38-39)      | 4                        | 6                               | 0.114              | 0.171       |
| (40-41)      | 7                        | 13                              | 0.200              | 0.371       |
| (42-43)      | 9                        | 22                              | 0.257              | 0.628       |
| (44-45)      | 5                        | 27                              | 0.143              | 0.771       |
| (46-47)      | 4                        | 31                              | 0.114              | 0.885       |
| (48-49)      | 2                        | 33                              | 0.057              | 0.942       |
| (50-51)      | 2                        | 35                              | 0.057              | 0.999 1.000 |

- a)  $P(MAR \ge 40) = 1.000 0.171 = 0.829 = 82.9\%$
- b)  $P(MAR \ge 50) = 0.057 = 5.7\%$
- c)  $P(40 \le MAR \le 50) = 0.942 0.171 = 0.771 = 77.1\%$
- 3.6 Using the curve data for a standard normal curve (Table B.1) requires standardization of the limits of the integral,

$$z = \frac{x - x}{S} = \frac{8 - 4}{2} = 2$$

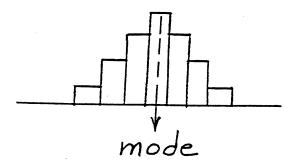
From Table B.1, the integral is the area to the right of F(z = 2), or 0.5 - 0.4772 = 0.0228.

- 3.7 For the data given:
  - a) The area under the curve must be 1.0 to qualify as a probability density function,

$$A = \int_{0}^{b} f(x)dx = \frac{b^{3}}{8} = 1.0$$

This gives b = 2.0

- b) This is the area between 0.0 and 0.5, or  $0.5^3/8 = 0.016$
- 3.8 The histogram is symmetric, has zero skew, and mean = median = mode.



Sketch for Prob. 3.8

Since area to right of mode is 50%, F(mode) = 50% and T = 2 yr.

3.9 Given 
$$x = 10.3$$
,  $s = 1.1$ ,  $C_v = 0.11$ ,  $n = 20$ 

$$S.E.(x) = s/\sqrt{n} = 1.1/\sqrt{20} = 0.245$$

$$S.E.(s) = s/\sqrt{2n} = 1.1/\sqrt{40} = 0.0174$$

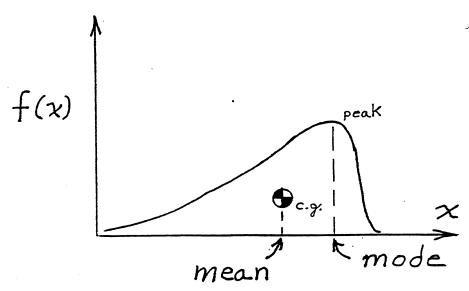
$$S.E.(C_v) = C_v \sqrt{1 + 2C^2}/\sqrt{2n} = 0.11\sqrt{1 + 2(.11)^2}/\sqrt{40} = 0.017$$

$$95 \% C.L.: z = \pm 1.96$$

$$x \pm 1.96 (S.E._x) = 10.3 \pm 0.48$$

$$= \{10.78 \text{ to } 9.82\}$$

- 3.10 Because the median divides the area in half, most of the area would be to the right of the median. The distribution is probably skewed right.
- 3.11 Sketch:



Sketch of p.d.f. for Prob. 3.11

- a) Left skewed
- b) Negative because Pearson skew =  $(\text{mean mode})/s_x$
- 3.12 For the 30,000 cfs value:

$$T_r = 60 \text{ yrs} = 20 \text{ yrs}$$
 $3 \text{ times}$ 

3.13 Frequency analysis:

| a) | m<br>rank | Peak<br>value | $\underline{F} = \underline{\frac{m}{10}}$ | $T_r = 1/F$ |
|----|-----------|---------------|--|-------------|
|    | 1         | 1000          | .1   | 10          |
|    | 2         | 900           | .2   | 5           |
|    | 3         | 800           | .3   | 3.33        |
|    | 4         | 700           | .4   | 2.5         |
|    | 5         | 600           | •  |             |
|    | 6         | 500           |  |             |
|    | 7         | 400           |  |             |
|    | 8         | 300           |  |             |
|    | 9         | 200           |  |             |
|    | 10        | 100           |  |             |

By interpolation, 4-yr value is

$$800 + \frac{4 - 3.33}{5 - 3.33} (100)$$

$$= 840 cfs$$

b) Using Table B.1,

$$Q_{4-yr} = \overline{Q} + K s_Q = 550 + .67(300) = 750 cfs$$

3.14 For an annual precipitation of 30 in.

a) 
$$P(x \ge 30) = G(30)$$
$$z = (30 - 27.6)/6.06 = 0.396$$
$$F(z) = 0.15392$$

$$G(30) = 0.5 - 0.15392 = 0.346$$

- b) Risk in 3 years =  $1 (1 G(30))^3$ = 0.720
- c) P(all three years) =  $G(30)^3 = 0.041$
- 3.15  $P(E_1 \cup E_2) = P(E_1) + P(E_2) P(E_1 \cap E_2)$ 
  - a) If  $E_1$  and  $E_2$  are independent,  $P(E_1|E_2) = P(E_1)$ and  $P(E_1 \cap E_2) = P(E_1) \times P(E_2)$  $P(E_1 \cup E_2) = 0.3 + 0.3 - 0.3 \times 0.3 = 0.51$
  - b) If dependent, with  $P(E_1|E_2) = 0.1$ ,

$$P(E_1 \cap E_2) = 0.1 \times 0.3 = 0.03$$
  
and  $P(E_1 \cup E_2) = 0.3 + 0.3 - 0.03 = 0.57$ 

3.16 
$$P(A) = 0.4$$
,  $P(no A) = P(\overline{A}) = 1 - 0.4 = 0.6$   
 $P(B) = 0.5$ ,  $P(no B) = P(\overline{B}) = 1 - 0.5 = 0.5$ ;

A and B independent

a) 
$$P(A \cap B) = P(A) \times P(B) = 0.4 \times 0.5 = 0.20$$

b) 
$$P(A \cap B) = P(A) \times P(B) = 0.6 \times 0.5 = 0.30$$

3.17 
$$P(E_1|E_2) = 0.9, P(E_2|E_1) = 0.2, P(E_1 \cap E_2) = 0.1$$
  
 $P(E_1) = P(E_1 \cap E_2)/P(E_2|E_1) = 0.1/0.2 = 0.5$   
 $P(E_2) = P(E_1 \cap E_2)/P(E_1|E_2) = 0.1/0.9 = 0.111$ 

- 3.18 Two random events that are:
  - a) Mutually exclusive:

A: Precipitation today exceeds 4 in.

B: Precipitation today does not exceed 3"

b) Dependent:

A: Precipitation today exceeds 4 in.

B: Runoff today exceeds 1 in.

c) Mutually exclusive and dependent:

A: Precipitation today does not exceed 4 in.

B: Runoff today exceeds 6 in.

d) Neither mutually exclusive nor dependent:

A: Today's precipitation exceeds 4 in.

B: Groundwater pumpage this year will exceed 3 acre-feet per acre

3.19 
$$P(A) = 0.4, P(B) = 0.5$$

a) 
$$P(A \cap B) = P(A) P(B|A) = 0.4(0.5) = 0.20$$

b) 
$$P(A \cap B) = 0.6(0.5) = 0.30$$

c) 
$$P(A \cap B) = P(A) P(B) = 0.6(0.5) = 0.30$$

## 3.20 For the given data:

a) Only if 
$$P(B|A) = P(B)$$

Now, 
$$P(B) = 0.6$$

$$P(B|A) = P(A \text{ and } B)$$
$$P(A)$$

Since P(A and B) = 0.2 and P(A) = 0.4

$$P(B|A) = \frac{0.2}{0.4} = 0.5$$
, Dependent

- b) No, mutually exclusive if P(A and B) = 0, but P(A and B) = 0.2
- c) P(B) = 0.6

d) 
$$P(\bar{A}) = 1 - 0.4 = 0.6$$

e) 
$$P(\overline{A} \text{ and } \overline{B}) = P(\overline{B}|\overline{A}) P(\overline{A})$$

From data, P(both) = 0.2

Check: 
$$P(\bar{A} \text{ and } \bar{B}) = 1 - P(E_1) - P(E_2) - P(E_3)$$

Possibles: Warm Mar Cold Mar Warm Mar Cold Mar Apr Flood Apr Flood Apr Dry Apr Dry P = 0.2 P = 0.4 P = 0.2 P = 0.2

f) 
$$P(B/A) = 0.5$$

g) to make them independent,

$$P(B|A) = P(B)$$
  
Since  $P(B) = 0.6$ 

$$P(B|A) = P(A \text{ and } B) = 0.2 = 0.5$$
  
 $P(A) = 0.4 = 0.5$ 

Change P(B) to 0.5, without changing P(A and B)

3.21 A: Flood B: Ice-jam

$$P(A \text{ and } B) = P(A|B)P(B)$$
, thus  $P(A \text{ and } B) < P(A|B)$   
and  $P(A \text{ and } B) < P(A)$ 

Also P(A or B) = P(A) + P(B) - P(A and B)

Also P(A) < P(A|B) because B < S

Ranking: Largest = P(A or B)

Second = P(A|B)

Third = P(A)

Fourth = P(A and B)

- 3.22 For the information given:
  - a) Both statements say the same thing when  $\underline{\underline{n}} = \underline{\underline{t}} = T_r$  years,

or 
$$T_r = 1$$
 yr

b) First:

$$(1 - 1)^{t-1} = (1 - 1)^{t-1} = (2)^2 = 4 = 0.444$$

Second: P = Probability annual precipitation value will not be equaled or exceeded in any single year,

$$P = 1 - F_x = 1 - \frac{1}{3} = \frac{2}{3}$$

$$\frac{n!}{r! (n-r!)} P^{n-r} (1-P)^{r} = \frac{3!}{1! (2)!} (\frac{2}{3})^{3-1} (1-\frac{2}{3})^{1} = \frac{4/9}{3}$$

3.23 For risk = 50%, 
$$R = 0.5 = 1 - (1 - 1/T)^2$$

for 2 consecutive yr

Solution gives T = 3.41 yr

For risk = 100%,  $R = 1 = 1 - (1 - 1/T)^2$ , T = 1 yr

3.24 For the temporary cofferdam:

- a) P(overtopping in any yr) = P(F) = 1/T = /20 = 0.05
- b) P(non-exceed in yr 1 and non-exceed in yr 2 and exceed in yr 3) = P(F) x  $P(F) \times P(F) = 0.95 \times 0.95 \times 0.5 = 0.451$
- c) Risk =  $1-(1-1/T)^n$  $1-(1-1/20)^5 = 0.226$
- d) P(non-exceed in 5 consecutive yr) =  $(1 - 1/20)^5 = 0.774$
- 3.25 For N = 33, median = 17th largest flow.

Defining Q as the annual peak:

- a) P(Q exceeds median) = 17/33 = 0.515
- b)  $T_r = 1/G(Q) = 1/0.515 = 1.94 \text{ yrs.}$
- c) G(Q) = 0.515 in any year.
- d) 1 G(Q) = 0.485
- e)  $P(Q \le median in all 10 yrs)$ =  $P(Q \cap Q \cap Q \cap Q...) = (0.485)^{10} = 0.00072$
- f)  $P(Q \ge \text{median at least once in 10 years})$ = 1 - (1 - G(Q))<sup>10</sup> = 0.99928
- g)  $P(Q_1 \text{ and } Q_2 \text{ exceed median})$ =  $P(Q_1) P(Q_2)$ = G(Q) G(Q) = 0.265
- h)  $P(Q_1 \text{ exceeds median and } Q_2 \text{ does not})$ G(Q)(1-G(Q)) = 0.250
- 3.26 For the temporary floodwall:
  - a) P(overtopping in any yr) = P(F) = 1/T = 1/20 = 0.05
  - b) P(non-exceed in 3 consecutive yr) =  $(1 P(F))^3$

$$= P(\overline{F})^3 = 0.95^3 = 0.857$$

- c) Risk =  $1-(1-1/T)^N = 1-(1-1/20)^3 = 0.143$
- d) P(exceed in 1st yr only or exceed in 2nd yr only or 3rd yr only)
  = P(in 1st yr only) + P(in 2nd yr only)
  + P(in 3rd yr only)

$$= P(F) \times P(\overline{F}) \times P(\overline{F}) + P(\overline{F}) \times P(F) \times P(\overline{F})$$
$$+ P(\overline{F}) \times P(\overline{F}) \times P(F)$$

$$= (0.05)(0.95)(0.95) + (0.95)(0.05)(0.95) + (0.95)(0.95)(0.05) = 0.135$$

e) P(exceed in 3rd yr exactly) = 
$$P(\overline{F}) \times P(\overline{F})$$
  
  $\times P(F) = (0.95)(0.95)(0.05) = 0.045$ 

## 3.27 The owner's acceptance level is:

Risk = 
$$1 - (1 - 1/T_r)^n = 0.25$$

Substitution of n = 20 gives  $T_r = 70$  yrs, thus the wall should be between 8.5 and 10.0 ft, or interpolating, 9.1 ft.

#### 3.28 For Oak Creek:

- a) Freq. = m/N = 3/60 = 0.05
- b) P(F) = freq. = 0.05
- c) T = 1/P(F) = 1/0.05 = 20 yr

d) 
$$P(\overline{F}) = 1 - P(F) = 1 - 0.05 = 0.95$$

- e) P(non-exceed in two consecutive yr) =  $P(\overline{F}) \times P(\overline{F}) = 0.95 \times 0.95 = 0.9025$
- f) P(one or more exceed in 20 yr)=Risk =  $1 - (1 - 1/T)^N$ =  $1 - (1 - 0.05)^{20} = 0.642$
- g) P(non-exceed in one yr and exceed in next yr)

$$= P(\overline{F}) \times P(F)$$
$$= 0.95 \times 0.05 = 0.0475$$

- h) Using Binomial Theorem, P(3 occurrences in 60 yr) = P(x in n) =  $[n!/x!(n-x)!]p^x(1-p)^{n-x}$ =  $[60!/3! 57!](0.05)^3(0.95)^{57} = 0.230$
- i) Same as part f).

### 3.29 For Anniston, Alabama,

Mean rain = 57.2 in.

Standard deviation = 15.5 in.

$$100$$
-yr X =  $57.2$  + K (15.5)

From Appendix B, K for 0.01 = 2.326,

$$X_{100} = 93.2$$
 in.

The 1988 depth of 99 inches was the greatest depth of record. It has an apparent recurrence interval of 23 years. If the rain is normally distributed,

$$99 = 57.2 + K_{99} (15.5)$$

Full Download: https://testbanklive.com/download/introduction-to-hydrology-5th-edition-viessman-solutions-manual/

$$K_{99} = 2.697$$

The area to the right of 2.697 is .49647, giving a recurrence interval of 1/.00353 = 283 years.

3.30 
$$P(\mu < x < \mu + \sigma) = \text{area from } z = 0 \text{ to } z = 1 = 0.3413 = 34.13\%$$

3.31 
$$P(\mu - 3\sigma \le X \le \mu + 3\sigma) = \text{area under standard normal from -3 to +3}$$

From Appendix C.1: 
$$P(\mu - 3\sigma \le x \le \mu + 3\sigma) = 2(.4987) = 0.997 \text{ or } = 99.74 \%$$

3.32 For Normal distribution of runoff:

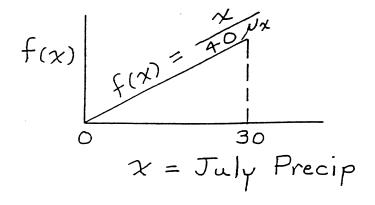
$$x = x + zs$$
,  $s = \sqrt{9} = 3$   
 $11 = 14 + 3z$ ,  $z = -1.0$ ,  $F(z) = 0.3413$   
 $P(x \le 11) = 0.5000 - 0.3413 = 0.1583$  in any yr  
 $P(x \le 11) = 0.5000 - 0.3413 = 0.1583 = 0.004 = 0.4\%$ 

3.33 From Table B.1, the standard variate, z, with area to the right of 0.330 is 0.44 (area left = F(z) = 0.5 - 0.33 = 0.17). Thus,

$$x = x + zs$$
  
= 5 + 0.44 (1.0) = 5.44

3.34 Since 
$$\mu = 0$$
,  $\sigma = 1$ , then  $\int_{-2}^{2} f(z)dz = 2(0.4772) = 0.9544$ 

3.35 Given:



Prob. 3.35 Definition Sketch

$$\mu_x \approx 30$$
 in.