Full Download: http://testbanklive.com/download/analog-circuit-design-discrete-and-integrated-1st-edition-franco-solutions-manu

CH. 2 – PROBLEM SOLUTIONS (UPDATED DECEMBER 16, 2013)

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2.1 Two conditions are necessary for successful B57 operation: (a) the emitter must be doped much more heavily than the base; (b) the emitter and collector must be separated by a thin contiguous base.

In the case of two discrete diodes, it is not known a priori whether (a) is met; (b) is certainly not met, as the two anodes are not contiguous; the holes injected from the emitter-acting anode would rather recombine with the electrons supplied by the "base" wire, than progress towards the collector-acting anode.

but condition (b) still isn't, as the two base regions, though thin, are not contiguous, but separated by interconnecting wires. The electrons supplied by those wires will recombine with the holes injected by the emitter, resulting in vistually sero collector when thus, $\beta_{\Sigma} \approx 0/T_B = 0$.

2.2 (a)
$$T_s = 10 \times 20 \times 10^8 \frac{1}{10^{-4}} 2 \times 10^{20} \frac{1.6 \times 10^{-19} \times 18}{10^{17}} = 0.115 f.$$

$$\beta = \frac{1.8 \cdot 10^{17} \cdot 1}{18 \cdot 10^{19} \cdot 1} + \frac{(10-4)^2}{2 \times 150 \times 10^{-9} \times 18} = \frac{1}{1000} + \frac{1}{540} = 351$$

2.3 (a)
$$\beta_{F} = 250 \Rightarrow 1/(1/x + 1/5) = 250$$
; $i_{B} = i_{BB} \Rightarrow x = y$; $1/(1/x + 1/5) = 250 \Rightarrow x = 500$

$$\frac{1}{500} = \frac{W_{B}^{2}}{27c_{n}D_{m}} = \frac{W_{B}^{2}}{2x150x_{10}^{7}9 \times 18} \Rightarrow W_{B} = 1.039 \text{ mm}$$

$$\frac{1}{500} = \frac{DP}{Dm} \frac{N_{AB}}{N_{DE}} \frac{W_{B}}{W_{E}} = \frac{1.8 \times 10^{17} \times 1.039 \times 10^{14}}{1.8 \times 10^{19} \times W_{E}} \Rightarrow W_{E} = 0.520 \text{ mm}.$$
(b)
$$\frac{x_{1}}{N_{2}} \frac{x_{2}}{2x_{10}^{2}0} = 940 \text{ mV}; \quad \phi_{c} = 700 \text{ mV}$$

$$\chi_{20} = \sqrt{\frac{26s}{9} \frac{\phi_{e}}{9N_{AB}}} \frac{N_{DE}}{N_{AB} + N_{DE}} = \sqrt{\frac{2x_{10}^{7} \times 0.94}{1.6x_{10}^{19} \times 10^{17}}} \frac{10^{19}}{10^{17} + 10^{19}} = 108 \text{ mm}$$

$$\chi_{10} = \frac{N_{AB}}{N_{DE}} \chi_{20} = \frac{108}{100} \approx 1.1 \text{ mm}$$

$$\chi_{20} = \sqrt{\frac{2x_{10}^{7} \times 0.7}{1.6x_{10}^{19} \times 10^{17}}} \frac{10^{15}}{10^{17} + 10^{15}} = 9.4 \text{ mm}$$

$$D_{1} = W_{E} + \chi_{1} = 520 \text{ mm} + (1.1 \text{ mm})\sqrt{1 - \frac{0.7}{0.94}} \approx 520 \text{ mm}.$$

$$D_{2} = W_{B} + \chi_{2} + \chi_{3} = 1.039 \text{ mm} + (108 \text{ mm})\sqrt{1 - \frac{0.7}{0.94}} \approx 520 \text{ mm}.$$

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(a)
$$T_s = (25 \times 10^{-4})(50 \times 10^{-4}) \frac{1}{10^{-4}} \times 2 \times 10^{20} \frac{1.6 \times 10^{-19}}{10^{17}} 8 = 0.32 \text{ fA}.$$

$$\beta_{F} = \frac{\frac{1}{3 \cdot 10^{17} \cdot 1 + \frac{(10^{-4})^{2}}{2 \times 100 \times 10^{-9} \times 8}} = \frac{1}{\frac{1}{267} + \frac{1}{160}} = 100$$

$$\beta_F = \frac{1}{K_2 W_B + K_3 W_B^2} \Rightarrow \beta_F = \frac{1}{\frac{0.5}{267} + \frac{0.5^2}{160}} = \frac{1}{\frac{533}{640}} + \frac{291}{640}$$

$$\beta_F = \frac{1}{K_3/N_E + 1/160} = \frac{1}{267 \times 2} + \frac{1}{160} = 123.$$

We affects both Is and BF, and helving it will double Is and increase BE bymare than a factor of 2.
WE affects only BF, and doubling it will habe the B-E diffusion component of IB, thus increasing BF.

2.5 (a)
$$IE \approx \frac{4-0.7}{3.3} = 1 \text{ m/A}$$
; $VEB = 0.076 \text{ km} \frac{10^{-3}}{4 \times 10^{-15}} = 0.682 \text{ V}$; $IE = \frac{4-0.682}{3.3} = 1.005 \text{ m/A}$
 $BF = \frac{1}{0.002 \times 0.001} = 167 \Rightarrow IB = \frac{1.005}{167+1} \approx 6 \text{ m/A}$

IB= 5-0.1 = 100 MA = IE. IC=0 JB + 3 KR About 14A of holes diffusing from 0.71 V + 1 B to E, and 99 MA of electrons diffusing from E to B.

It = 100 MA (NIMA holes from B to E, and ~ 99 MA electrons from E to C). 4Ic Ic+IB = 100 IB+ IB = 100 MA > IB = IMA (holes from B to E plus holes recombining with elons within B). Ic ~ 99,4A (electrons from Eto Bto C).

100, MA | \$43kr | LE IB = 100, MA (holes from B to E plus holes recombining with el. no within B).

IC= B= IB = 100 × 0. 1= 10 mA (electrons from E to B). TE= IB+Ic=10.1 mA

VB = -5-0.8=-5.8V; IE=IL= 500MA; IB=IE/(BF+1)=500/81=6.17MA; IC=IE-IB=494MA. (a) $i_{01} = \frac{1}{100} = 10 \text{ mA}$; $i_{02} = 0$; NI = 100 + 1000 = 1000 = 1000 = 1000 = 1000 = 1.72 V; $i_{1} = 10/151 = 66.2 \text{ mA}$.

(b) $i_{01} = 0$; $i_{02} = 10 \text{ mA}$; $V_{I} = 100 - 1000 = 1000 = 1000 = 1.70 \text{ V}$; $i_{IZ} = 10/101 = 1000 = 1.70 \text{ V}$; $i_{IZ} = 10/101 = 1000 = 1000 = 1.70 \text{ V}$.

(c) $i_{01} = 50 \text{ mA}$; $i_{II} = 10.33 \text{ mA}$; $v_{I} = 10.70 = 1$

[2.9] (a) $\lambda_{C2} \approx i\epsilon_{Z=} \sqrt{0}/R_L = 1/8 = 125 \text{ mA}$; $i_{I} = \frac{125}{101 \times 51}$ $\approx 24 \text{ mA}$; $\lambda_{C1} = 100 \times 24 = 2.43 \text{ mA}$. $VI = 1 + 0.026 \left[\frac{2.43 \times 10^{-3}}{10 \times 10^{-15}} + \frac{125 \times 10^{-3}}{10^{-12}} \right] = 1 + 1.346 = 2.346 \text{ V}$.

(b) $\lambda_{C2} \approx \frac{4}{8} = 500 \text{ mA} \left(= 2 \times 2 \times 125 \text{ mA} \right)$; $\lambda_{I} \approx 97 \text{ mA}$; $\lambda_{I} \approx 4 + 1.346 + 2 \left(18 + 18 \right) \times 10^{-3} = 5.418 \text{ V}$ (c) $\lambda_{C2} \approx 2A \left(= 16 \times 125 \text{ mA} \right)$; $\lambda_{I} \approx 0.388 \text{ mA}$. $\lambda_{I} = 16 + 1.346 + 2 \left(18 + 18 + 18 + 18 \right) \times 10^{-3} = 17.490 \text{ V}$.

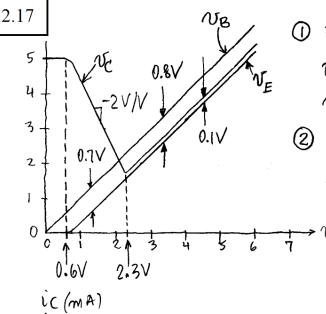
2.10 (a) $\hat{i}_{CZ} = \hat{i}_{EZ} = 1/4 = 250 \text{ mA}; \ \hat{i}_{E} = \frac{250}{101 \times 41} = 60.4 \text{ mA}; \ \hat{i}_{CI} = |00 \times 60.4 = 6.04 \text{ mA}.$ $N_{E} = -1 - 0.026 \left[ln \frac{6.04 \times 10^{-3}}{5 \times 10^{-15}} + 1.5 ln \frac{250 \times 10^{-3}}{100 \times 10^{-12}} \right] = \\ = -1 - (0.723 + 0.844) = -2.567 \text{ V.}$ (b) $\hat{i}_{CZ} = \hat{i}_{EZ} = 5/4 = 1.25 \text{ A} (= 250 \times 10/2 \text{ mA}); \ \hat{i}_{E} = 60.4 \times 10/2 = 302 \text{ mA}; \ N_{E} = -1 - \left[(723 + 60 - 18) \text{mV} + (844 + 1.5 \times 60 - 1.5 \times 18) \right] \text{mV} = -1 - (0.765 + 0.907) = -2.672 \text{ V.}$

[2.11] (a) $|x|0^{-3} = 10^{-5} e^{\sqrt{8}E/26mV} (1+\frac{7}{15}) \Rightarrow VBE = 917mV.$ (b) $IC = (1.0mA) \times [(1+12/75)/(1+5/75)] = 1.0875mA$ $IC = (1.0mA) \times [(1+1/75)/(1+5/75)] = 0.95mA.$ (c) $\Delta T = -25 \circ C \Rightarrow \Delta V_{BE} = -2(-25) = +50mV \Rightarrow$ VBE = 717+50 = 767mV. $IC = 0.7mA = (1mA) \times (2/10) \Rightarrow \Delta V_{BE} = +18-60 = -42mV;$ $\Delta T = 50-25 = +25mV \Rightarrow \Delta V_{BE} = -2(25) = -50mV;$ $\Delta V_{Gnet}) = -42-50 = -92mV;$ VBE = 717-92 = 675mV. $\Delta V_{Gnet}) = 18+18-2(40-25) = 6mV;$ VBE = 773mV.

2.12 (a) 500 x 10 = 2 x 10 - 15 e VEB / 26 (1+ 4) > VEB = 680 mV. (b) Tc = (500 μΛ) x [(1+ 1/50)/(1+ 4/50)] = 472 μΛ. Tc - (500 μΛ) [(1+8/50)/(1+4/50)] = 537 μΛ. (c) 200 μΛ = 500 μΛ × 2/10 > ΔVEB = +18-60 = -42 mV; ΔΤ= 75-25 = 90 °C; ΔVEB = (2mV) 50 = -100 mV; ΔVEB (60) = -42-100 = -142 mV; VEB = 680-142 = 538 mV. (d) ΔΤ = 55-25 = 30 °C. Of we were to keep Tc constant at 500 μΛ; μνι d have to decrease VeB ly 30×2=60 mV, η lower it to 680-60 = 620 mV. We are vistend hering it constant at a value 60 mV higher, midicating a 10-fold increase in Tc, so Tc = 10×500 = 5 m Å. [2.13] (a) $\pm_B = \frac{5-0.7}{300} = 14.3 \text{ MA}$; $\pm_C = \beta_F \pm_B = 120 \times 14.3 \text{ MA}$; $\pm_C = 1.720 = 1.56 \text{ V}$. (b) Shorting ant k_2 changes $\pm_C = 5-2 \times 1.720 = 1.56 \text{ V}$. Since $\pm_C = \frac{1.720}{1.720} = \frac{1.76}{100}$, $\pm_C = \frac{1.720}{1.720} = \frac{1.720}{1.7$

2.14 (a) $T_{c} = \frac{5-1}{2} = 2mA$, $T_{B} = \frac{5-0.71}{300} = 14.3mA$ $\Rightarrow \beta_{F} = \frac{2}{0.0143} = 140$. $T_{s} = T_{c}/e^{V_{BE}/V_{7}} = \frac{2}{100} + \frac{3}{100} = \frac{3}{100} =$ 2.15 (a) $I_B = \frac{6 - 0.69}{470} = 11.3 \mu A$; $I_C = \frac{6 - 1}{3} = \frac{5}{3} \mu A$; $P_F = (5/3)/0.0113 = 147.5$. $(5/3) \times 10^{-3} = I_S e^{690/26} \Rightarrow$ $I_S = 5 \text{ } f_A \cdot (6) V_A/I_C = \Delta V_C/\Delta I_C \Rightarrow V_A = \frac{5 - 0}{0.1 \times 5/3} \frac{5}{3} = 50 \text{ } V$. (c) $I_C = 3.5/10 = 0.35 \mu A$; $I_B = \frac{6 - 0.7}{20} 0.765$; $P_A = 0.35/0.765 = 1.3$.

2.16 (a) $V_{BC}=0 \Rightarrow T_{C}=(10.7-0.7)/10=1.000 \text{ mA};$ $\beta_{F}=1000/8=125.$ (b) $V_{BC}=-10 \text{ V} \Rightarrow \chi_{p}=20\text{nm}\sqrt{1-\frac{10}{0.8}}=73.5 \text{ nm}.$ $V_{B}=500-73.5=426.5 \text{ nm}.$ $T_{C}=1\text{mA}\frac{500}{426.5}=1.172\text{mA}.$ (c) $V_{0}=\frac{4V_{C}}{4T_{C}}=\frac{10}{0.172}=58 \text{ m}=\frac{V_{A}}{47}\Rightarrow V_{A}=60 \text{ V}.$



① FOR $V_{\pm} < V_{BE(EOC)} = 0.6V_{j}$ the BJT is in cutoff; $V_{C} = V_{S} = 5V_{j}$, ic = 0.

(2) Raising of above 0.6V turns the BJT on.

Imitially, it is

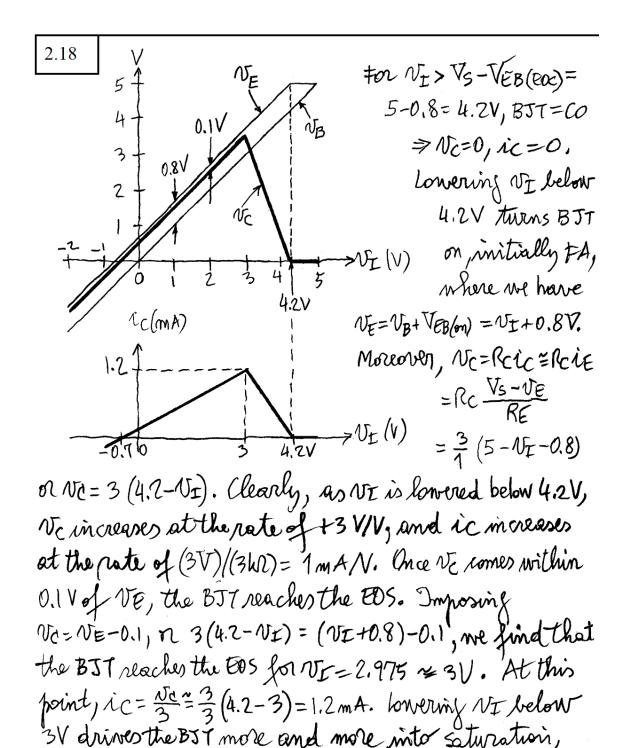
If in FA, where $V_E = V_B - V_{BE}(on) = V_L - 0.7V$.

Moreover, $V_C = V_S - R_{C}i_C$ $\leq V_S - R_C i_E = V_S - R_C \times C$ $\leq V_L - V_B = (on)$, or

 $NC = V_S + \frac{RC}{RE}V_{BE}(on) - \frac{RC}{RE}V_{I}$. Clearly, the plot of V_C v.s. V_I has a slope of -Rc/RE = -2V/V.

3 The BJT reaches the EOS when $\frac{V_E}{7} = \frac{5 - (V_E + 0.2)}{2}$, or $V_E = 1.6V$. At this point, $V_C = V_E + 0.2 = 1.8V$, and $V_B = 1.6 + 0.7 = 2.3V = V_I$. Also, $N_C = (5 - 1.8)/2 = 1.6 \text{ mA}$ (1) As me keep in creasing V_I , the BJ saturates, and $V_E = V_I - 0.8V$, $V_C = V_E + 0.1 = V_I - 0.7V$, and $i_C = (5 - V_C)/2 = [5 - (V_I - 0.7)]/2 = (5.7 - V_I)/7$. Clearly, ic now decreases with V_I .

(3) As NI reaches 5.7V, ic drops to sero. For NI>5.7V, ic becomes negative. The B-Cirunction is forward liased, and ic flows out of the collector!



and No=No-0.1= NI+0.8-0.1= NI+0.7V, NC=NC/Rc=

(VI+0.7V)/(3hr). Once NI is lowered to -0.7V, ic becomes

0, and turns negotive (i.e. flowers into the FB B-C

junction) for NI <-0.7V.

2.19 [V, mA, kr].

1. NS < 0.7V > BJT=CO > ic=iB=0, NC=-5V.

7. V5>0.7V >> BTT=ON, initially FA:

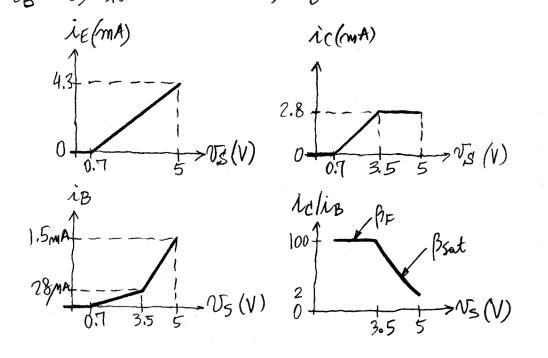
 $\hat{N}_{E} = \frac{N_{S} - 0.7}{1}, \hat{N}_{B} = \frac{\hat{I}_{E}}{\hat{D}_{F} + 1} = \frac{N_{S} - 0.7}{10|x|}, \hat{N}_{C} = d_{P}\hat{I}_{E} = \frac{100}{101} \frac{N_{S} - 0.7}{1} \approx \hat{I}_{E} = \frac{N_{S} - 0.7}{10|x|}, \hat{N}_{C} = -5 + 2(\frac{N_{S} - 0.7}{1}).$

(3) When No reaches NEB-VEC (EDS) = 0.7-0.1 =0.6V, BJT reaches EOS. At this point,

Ic(tos)= 0.6-(-5) = 2.8 mH, Vs(EOS) = 0.7+1 × IE(EOS) =

0.7+1×IC(05)=0.7+2.8=3.5V; IB(05)=2.8=28 MA.

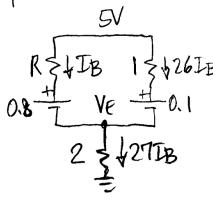
(4) For $N_S > 3.5V$, BJT=Seat: ic = Ic(e05) = 2.8 mA, $N_E = \frac{N_S - 0.7}{1}$, $i_B = i_E - i_C = \frac{N_S - 0.7}{1} - 2.8 = (N_S - 3.5) \text{ mA}$. $\frac{i_C}{i_B} = \frac{2.8}{N_S - 3.5}$. For $N_S = 5V$, $\frac{i_C}{i_B} = \frac{2.8}{N_S} = 1.86$.



2.20 (a)

KVL: Va=RaTa+VCE+RETE => 5=1BFTB+2+2(BFH)IB; KVL: Vcc=RBFB+VBE(m)+REJE >> 5=300 FB+0.7+2(Bp+1) IB; >3=(3/3+12) IB, 4,3=(302+2/3+) IB >> $\frac{3}{4.3} = \frac{3.05+2}{302+2.05} \Rightarrow 05 = 130.$

(b) kVL: 5=1IC+0.2+2IE ≥ dFFE+0.2+2 IE ≥ 0.2+3IE => IE = (5-0.2)/3=1.6 mA; VE=2x1.6=3.2V, VB=3.2+0.7= 3.9V; FB=1.6/131=12.2MA; RB=(5-3.9)/0.0122=90M. (c) Boot = 130/5=26 => IC=26 JB; IE=27 DB.



VE=2×2778=54 B. R\$\f\text{IB} \langle \frac{1}{5} \delta \frac{1}{26} \text{IB} \rangle \frac{1}{5} = \frac{1}{26} \text{IB} + 0.1 + 54 \text{IB} \Rightarrow \text{I}_B = \frac{61.25}{18} = \frac{61.25}{18} \text{A.}

\[
\text{VB} = \frac{1}{5} \delta \times 0.062125 + 0.8 = \frac{3.4075}{1.00} \text{V.}

\] R=(5-3.4075)/0.06175=14.6M.

(a) [V, kn, mA]. KVL: 5=3IE+1+1Ic, or 4=3(BF+1) IB+BFIB=(4B++3) IB KVL: 5=3IE+0.7+180IB,02 4.3 = 3 (BF+1) IB+180 IB = (3BF+183) IB Take the ratio of the two egns: 43 = 4BF+3 > BF=138

Swapping RE and Re causes the BJT To Saturate.

 $K(L: \frac{0-VE}{1} = \frac{VE-0.8-(-5)}{180} + \frac{Ve-0.1+5}{3}$ > VE=-1.237 V. IE=1.237 mA; Ic= 1.221mA; IB= 16.5 MA. Boot = 1.221 = 74 < 138 (=BF).

2.22 (a) KVL: TS= VBE(en) + R, IB+R2(IB+Ic).

In FA, 5=0.7+20IB+3(1+150) IB>IB=9.09 MA: IC=150×9.09=1.36 MA; IE=1.372 MA; KVL: VC=0.7+20×0.00909-R3×1.36=0.881-R3×1.36.

Vc(min)=VcE(E05)=0.2√⇒0.2=0.881-N3(max)×1.36 >> 0≤R3 ⊆ 0.5 kΩ.

(b) R3= 2×0.5=1 M => BJT= Sot >> VCE=0, IV, VBE=0.8 V.

 $\frac{5-\sqrt{x}}{3} = \frac{\sqrt{x}-0.8}{20} + \frac{\sqrt{x}-0.1}{1} \Rightarrow \sqrt{x} = 1.306 \text{ V}.$

JEN = 25.3 MA, IC = 1.206 MA, → IB = 25.3 MA, IC = 1.206 MA, Bout = 1.206/0.0253 = 48.

(c) Ic=0 >> Psot=0/IB=0.

[2.23] (a) Assume FA) and Check. By inspection, $T_{Rz}=T_B+T_C$ = $(\beta_F+1)T_B=151T_B$. kVL: $q=20(151T_B)+100T_B+0.7 \Rightarrow T_B=2.66\mu A$, $T_C=150T_B=0.399 mA$) $T_C=151T_B=0.402 mA$. By kVL efain, $T_C=150T_C=0.402 mA$.

(6) Assume Saturation, and check. KCL:

$$\begin{bmatrix} V_{1}W_{1}\gamma_{M}A \end{bmatrix} : \begin{array}{c} 9 \\ 9 \\ \hline 1 \end{array} = \begin{array}{c} V_{X} - 0.1 \\ \hline 1 \end{array} + \begin{array}{c} V_{X} - 0.8 \\ \hline 100 \end{array} \Rightarrow V_{X} = 6.73V. \\ I_{B} = \begin{array}{c} 6.73 - 0.8 \\ \hline 100 \end{array} = \begin{array}{c} 59.3 \text{ MA} \end{array}$$

$$I_{C} = \begin{array}{c} 6.73 - 0.1 \\ \hline 3 \end{array} = 2.22 \text{ Im} A$$

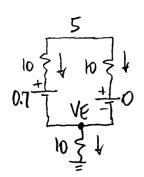
$$I_{E} = I_{C} + I_{B} = 2.28 \text{ mA}$$

Psat= Ic/IB = 2.221/0.0593=37 < 150=> Sat!

2.24

(a) [V, MA, KR]. Assume FA. KVL:

18 10 \$ VIC 5 0 10 + 0.7- 101 IB 5=10IB+0.7+10(10IIB) = IB=4.2MA IC=0.422mA; IE=0.426 anA VB=5-10IB=4.958V; VE=4.26V Vc=10-10×0.422=5.78 V VCE=5.78-4.26=1.52V>0.2V=FA!

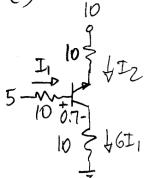


Now BIT is saturated.

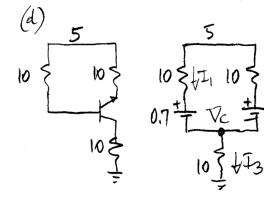
kcl:

$$\frac{5 - (VE + 0.7)}{10} + \frac{5 - VE}{10} = \frac{VE}{10}$$
 $\Rightarrow V_E = 3.1 \text{ V}.$

 $F_{E}=0.31 \text{ mA}$; $F_{B}=0.12 \text{ mA}$; $F_{C}=0.19 \text{ mA}$. Poset = $\frac{0.19}{0.12}=1.6$.



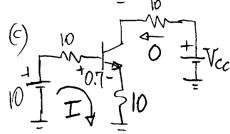
 $5 = 10I_1 + 0.7 + 6I_1 \Rightarrow I_1 = 61.4 \mu A$ $I_2 = 5I_1 = 307 \mu A$; $6I_1 = 369 \mu A$. $V_B = 5 - 10I_1 = 4.39V$; $V_C = V_B - 0.7$ = 3.69V; $V_E = 10 - 10I_2 = 6.93V$ $V_{EC} = 6.93 - 3.69 > 0.2V \Rightarrow RA!$



BJT is in reverse-mode Saturation. Equivalent Circuit is similar to (b). $V_C = 3.1V$, $I_1 = 0.12 \text{ mA}$ $I_2 = 0.19 \text{ mA}$, $\beta_{sot} = 0.19/0.12 = 1.6$. 2.25 [V, mA, kn].

KVL: 10=10(100IB)+1+10(10IB) +100IB => IB = 4.478 MA; +1 VE=10×10IDB = 4.522 V; VB=VE+0.7V +101IB = 5.22 V; VBB=VB+100DB = 5.67 V.

LVL: 10 = 10(5IB) + 1 + 10(6IB) $5IB = 81.81 \mu A$ $V_{c} = 10 \times 6IB = 4.91 V; V_{B} = 5.61 V$ $V_{BB} = 5.61 + 100 \times 0.081 = 13.8 V.$



 $J_{C=0} \Rightarrow J_{B=JE} = I$. kVL: $10=10I + 0.7 + 10I \Rightarrow I = 0.465 mA$ $\Rightarrow V_{E} = 4.65V$, $V_{B} = 5.35V$. $\forall 0 \downarrow c = 0$, $V_{CC} = V_{B} - 0.65 = 4.7V$.

(d) 5 10.5IE
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IB=1.5 IE \Rightarrow Ic=-0.5 IE (owt of Collector) 10.5 IE \Rightarrow Boot = $(0.5 \text{ DE})/(1.5 \text{ IB}) = -\frac{1}{3} < \beta_F \Rightarrow \text{Soot}$. \Rightarrow VBC = VBE = 0.7 V \Rightarrow 10 IE = 5+10 (0.5 IE) \Rightarrow IE = $|\text{Im} A \Rightarrow \text{V}_{\text{BB}} = 10 (1.5 \times 1) + 0.7 + 10 (1) = 25.7 \text{ V}$.

(a) [V, mA, kn]. Aroune FA: kVL: $VE = 12 = 2 \times 151 \text{ TB} + 0.7 + 3 \text{ FB} + 6$ $\Rightarrow \text{TB} = 17.4 \text{ MA}$; FC = 2.61 mA, VE = 2.62 mA, VB = 6.052 V, VE = 6.752 V, VC = 2.607 VVEC=4.14V>0.1V > FA! (b) 13/IE 10=1x5TB+0.7+3TB+5 => TB=0.5375 mA Tc'=4x0.5375=2.15 mA De1=5 x0,5375=2.6875MA VB=5+3×0.5375=6.6125V; Vc=6.6125+0.7=7.3125V; VE=2×2,15=4,3V, 7,3125-4,3>0,1> RA! (c) Assume Sat: 6-VE = VE-0.7 + VE-0 PVE=1.736 V Vc=1.736 V Ic=1.736 MA

TB=1.036/3=0.345 MA; Bat=1.736/0.345 = 5< B= >Sot!

2.28 [V, MA, KN]. Assume Q1=Q2=FA. IEZ=51 0.5=0.51 mA.

| 10 | kvl: $V_{E2}=10-10\times0.51=4.9V$. kvl: $V_{E1}=10=10\times0.51=4.9V$. kvl: $V_{E2}=4.9-0.7=4.2V=V_{C1}$. kcl: $V_{C1}=\frac{J_{B2}}{J_{C1}}$ | $Q_{C1}=\frac{J_{B2}}{J_{C1}}$ | $Q_{C1}=\frac{J_{C2}}{J_{C1}}=\frac{4-0.7}{3}-0.5=0.6$ mA. kcl: $V_{C1}=\frac{J_{C1}}{J_{C1}}$ | $V_{C1}=\frac{J_{C1}}{J_{C1}}$ | $V_{C1}=\frac{J_{C2}}{J_{C1}}$ | $V_{C1}=\frac{J_{C1}}{J_{C1}}$ | $V_{C1}=\frac{J_{C1}}{J_{C1}$

Ohm: R= 10-4.2 = 10.0 ka. Check: VCE1=4.2-(4-0.7)>0.2V

>Q=ta. VEC2=4,9-(4-0.7)>0.2V > Qz=FA.

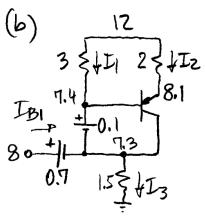
IHV = IB) = IC1/BA= (33/56)/55 = 10.7 MA.

2.29 [V, mh, ka]. Assume Q= Q= FA, and check. Ve1=Va=

(a) $\frac{12}{3}$ $\frac{1}{4.3}$ $\frac{1}{4.3}$ $\frac{1}{4.3}$ $\frac{1}{4.3}$ $\frac{1}{4.3}$ $\frac{1}{4.3}$ $\frac{1}{4.3}$ $\frac{1}{4.3}$ $\frac{1}{4.3}$

5-0.7=4.3 V. Ignoring base currents, $I_3 = I_{E|} + I_{C2} \cong I_1 + I_{Z}, \text{ or}$ $\frac{4.3}{1.5} = \frac{12 - V_{C1}}{3} + \frac{12 - (V_{C1} + 0.7)}{2}$ $\Rightarrow V_{C1} = 8.14 \text{ V} \Rightarrow I_{C1} \cong I_1 = \frac{12 - 8.14}{3} \cong 1.29 \text{ mA}; I_{C2} \cong I_2 = \frac{12 - (8.14 + 0.7)}{2} \cong 1.29 \text{ mA}; I_{C2} \cong I_2 = \frac{12 - (8.14 + 0.7)}{2} \cong 1.29 \text{ mA}; I_{C2} \cong I_{C1} \cong I_{C2} \cong I_{C1} \cong I_$

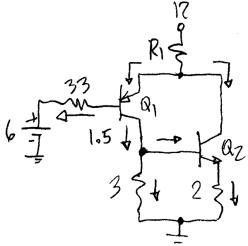
1.58 mA; $V_{eq} = 8.14 - 4.3 = 3.84 \text{V} (>>0.1V \Rightarrow Sat)$; $V_{ec2} = (8.14 + 0.7) - 4.3 = 4.54 \text{V} (>>0.1V \Rightarrow Sat)$. Consequently, $Q_1 = Q_1(1.29 \text{ mA}, 3.84 \text{V}), Q_2 = Q_2(1.58 \text{ mA}, 4.54 \text{V})$.



Assume $Q_1 = Sat$, $Q_2 = TA_1$, and check. $Ve_1 = Vc_2 = 8 - 0.7 = 7.3V$; $T_3 = 7.3/1.5 = 4.87$ MA; $Vc_1 = VBz = 7.3 + 0.1 = 7.4V$; $Ve_2 = VBz + 0.7 = 8.1 \text{ V. } I_1 = (17 - 7.4)/3 = 1.53$ MA; $I_2 = (17 - 8.1)/2 = 1.95$ MA. $Q_2 = Q_2(1.95$ MA) 0.8V), FA. KCLi

 $IB_1 = I_3 - (I+I_2) = 4.87 - (1.53 + 1.95) = 1.38 \text{ m A} \cdot Fa/IBI = I/IBI = 1.53/1.38 = 1.1 \Rightarrow Q_1 = \text{Sat, and } Q_1 = (1.53 \text{ m A}, 0.1 \text{ V}).$

2.30 (a) [V, m A, M]: KCl: 15= I3hr+ IBZ= I3hr+ IEZ/(B2+1)

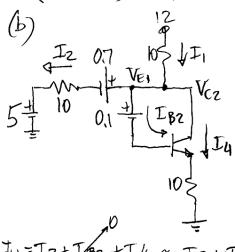


JBI = JCI/BI = 1.5/50 = 0.03mA; $VBI = 6+33 \times 0.03 = 6.99V$; VEI = VBI + 0.7 = 7.69V. RI = (12-7.69)/3.34 = 1.3 MR. Chech: $VECI = (12-1.3 \times 3.34) - 4.39 = 3.3V >> 0.1V \Rightarrow FA$. $VCEZ = (12-1.3 \times 3.34) - (4.39-0.7) = 4V \Rightarrow 0.1V \Rightarrow FA$. (b) The base currents can be ignored, except when calculating the voltage drop across R_2 . Thus, $VCI = 3 \times 1.5 = 4.5V$; TEZ = (4.5-0.7)/2 = 1.9 mA; TRI = 1.5 + 1.9 = 3.4 mA; RI = (12-7.69)/3.4 = 1.27 MP = 1.3 MP.

[V,m A, M]. Assume Q= RA, and chech.

Icz = 0.63-0.35= 0.28 mA.

VEG= 5.7-3.5=2.2V >> QIV > FA; VCEZ=5.7-(3.5-01)= 29V>> QIV => FA. Thus, Q= Q1(0.35mA, 2.2V); Qz= Qz (0.28mA, 2.9V).



 $\frac{12 - Vx}{10} = \frac{(Vx - 0.7) - 5}{10} + \frac{(Vx - 0.1) - 0.7}{10} \Rightarrow Vx = 6.16 V.$ $IB_1 = I_2 = \frac{(6.16 - 0.7) - 5}{10} = 0.046 \text{ mA}; I_{C2} = I_4 = \frac{(6.16 - 0.1) - 0.7}{10}$ =0.536 mA. Ic1=IBZ= Tc2/BF2. Assuming BF2>100, Me have Ic1 < 0.536/100 = 5.36μA >β sol1 < 5.36/46.6 ~0.1 => Q1 = Sat. Thus, Q1=Q1 (<5.36MA, 0.1V), and Qz=Qz(0.536mA, 0.8V).

| 2.32 | [V,mA, hn]. Use kVL, kcl, Ohm's law rejeatedly. | Vcc = RyIcz + Vecz (EOS) + R5I2 = (R4+R5) Icz + Vecz (EOS) \Rightarrow | 15 = 2.2 Icz + 0.2 \Rightarrow Icz = 6.72 mA. | VEZ = 1×6.72 = 6.72 V; VBZ = 6.72 - 0.7 = 6.027 V = Vc1. | IBZ = 6.72/100 = 67.27 MA | Ic1 = (15 - 6.027)/30 + 62.27 × 10^{-3} = 0.3663 MA. Assume Q= FA. | IBI = 0.3663/100 = 3.66 MA | VBI = VI - RIIBI = 5 - 110 × 3.66×10^{-3} \approx 4.6 V | VEI = 4.6 - 0.7 = 3.9 V | IEI \approx Ic1 = 0.37 MA | R3 = 3.9/0.37 = 10.5 &C. | Vc21 = 6.027 - 3.9 \Rightarrow 0.7 \Rightarrow QI = FA.

Consider Q, first, and assume FA. KVL, kCL, D: IBI = 5-0.7 = 2.23 MA VBI = 5-110 × 2.23 × 103 = 4.75 V; VEI = 4.05 V

ICI=100×2.73=0.223 ml

Vc1=15-30×0.223=8.31 V

 $V_{CE1} = 8.31 - 4.05 \Rightarrow 0.2 \Rightarrow Q_1 = FA. \quad Eguivalent Cht:$ $Ascume Q_2 = FA. \quad 1.72$ $30 \quad 0.74 \quad vol5$ $Q_2 \quad V_{B2} = 8.31 + 30 \times 39.6 \times 10^3 = 9.5V$ $8.31 \quad V_{B2} = 9.5 + 0.7 = 10.2 V$ $V_{E2} = 9.5 + 0.7 = 10.2 V$ $V_{E2} = 9.5 + 0.7 = 10.2 V$ $V_{E2} = 9.5 + 0.7 = 10.2 V$

VC2=1×3.96=4V. VEC2=10.2-4>70.2=> QZ=KA.

For VI>VCC-VEB(EOC) = 5-0.6 = 4.4V, the BJT is in cutoff. Lowering VI below 4.4V drives the BJT in FA:

Fix
$$N_{I} = V_{CC} - V_{EB} - R_{B}i_{B}$$

$$= V_{CC} - V_{T} m \frac{V_{O}R_{C}}{I_{S}} - R_{B} \frac{V_{O}R_{C}}{B_{F}}$$

$$= 5 - 0.026 m \frac{V_{O}}{10^{3} \times 10^{15}} - \frac{10}{1} \frac{V_{O}}{80}, \text{ or}$$

$$V_{I} = 5 - \frac{V_{O}}{8} - 0.026 m (10^{12} V_{O}).$$

$$V_{CC} - V_{EC}(s_{O}t) = 5 - 0.1 = 4.9 \text{ V}.$$

This occurs for VI=5-49-0.076h (1012×4.9)=3.628V.

(c)
$$\frac{dv_{I}}{dv_{I}} = -\frac{1}{8} \frac{dv_{0}}{dv_{I}} - 0.026 \frac{1}{10^{12}v_{0}} 10^{12} \frac{dv_{0}}{dv_{I}}$$
, or $\frac{1}{10^{12}v_{0}} \frac{dv_{0}}{dv_{I}}$

2.35 (a) KVL: VI=RBiRB+VBE=RB(iB+VBE)+VBE =
RBiB+(HRB/RBE) VBE.

(b) $N_{I} = 10^{4} \left(\frac{5-N_{0}}{10^{3}}\right) / 100 + \left(1+\frac{10}{5}\right) 0.026 \, \text{m} \frac{5-N_{0}}{10^{3} \times 2 \times 10^{-15}}$ $N_{I} = \frac{5-N_{0}}{10} + 0.078 \, \text{lm} \frac{5-N_{0}}{2 \times 10^{-12}}.$

(c) $V_{\pm} = \frac{5-2.5}{10} + 0.078 \text{ ln} \frac{5-2.5}{2\times10^{-12}} = 0.75 + 2.173 = 2.423 \text{ V}$ (Shifted to the right by about $2\nabla_{8E}$'s).

(d) $\frac{dv_{T}}{dv_{T}} = \frac{1}{10} \frac{dv_{0}}{dv_{T}} + 0.078 \frac{7 \times 10^{-12}}{5 - v_{0}} \left(-\frac{1}{2 \times 10^{-12}} \frac{dv_{0}}{dv_{T}} \right) \Rightarrow$ $1 = -\frac{\alpha}{10} - 0.078 \frac{\alpha}{5 - v_{0}} \Rightarrow \alpha = -10 \frac{5 - v_{0}}{5.78 - v_{0}}.$

@NO=2.5V, a=-7.62VV. In the example, a=-9.06VN. Reduced game stems from the presence of RBE, which forms an input voltage divides with RB.

2.36

(Q) REB = $V_{I} = 5 - V_{EB} - R_B (i_B + \frac{V_{EB}}{R_{EB}})$ $= 5 - R_{BiB} - (1 + \frac{R_B}{R_{EB}}) V_{EB}, i_B = \frac{i_C}{80} = \frac{N_0}{80 \times 10^3}$ $V_{I} = 5 - R_{BiB} - (1 + \frac{R_B}{R_{EB}}) V_{EB}, i_B = \frac{i_C}{80} = \frac{N_0}{80 \times 10^3}$ $= 5 - R_{BiB} - (1 + \frac{R_B}{R_{EB}}) V_{EB}, i_B = \frac{i_C}{80 \times 10^3} = \frac{N_0}{80 \times 10^3}$ $= 5 - R_{BiB} - (1 + \frac{R_B}{R_{EB}}) V_{EB}, i_B = \frac{i_C}{80 \times 10^3} = \frac{N_0}{10^4} \times 10^{-15} \times 10^$

For No= 2.5V, gain = -10.7 V/V

2.37 (a)
$$[V_{1} m A_{1} k n]$$
. $N_{I} = V_{C} - N_{EB} - R_{B} (i_{B} + \frac{N_{EB}}{R_{CB}})$

$$= V_{C} - R_{B} i_{B} - (1 + R_{B}/R_{EB}) N_{EB}$$

$$= 5 - 10^{4} i_{B} - 2 N_{EB}$$

$$= 5 - 10^{4} i_{B} - 2 N_{EB}$$

$$N_{I} = 5 - \frac{N_{O}}{25} - 0.052 ln(0^{11} N_{O})$$

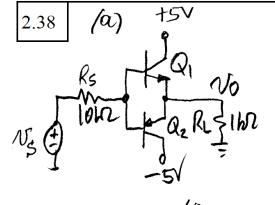
$$N_{I} = 5 - \frac{2}{25} - 0.052 ln(0^{11} N_{O})$$

$$N_{I} = 5 - \frac{3}{25} - 0.052 ln(0^{11} N_{O})$$

$$N_{I} = 5 - \frac{3}{25} - 0.052 ln(0^{11} N_{O})$$

$$N_{I} = (3 - 2)/(3.506 - 3.567) = (1 V)/(-61 mV) = -16.4 V/V$$

$$N_{I} = (3 - 2)/(3.506 - 3.567) = (1 V)/(-61 mV) = -16.4 V/V$$



VICIO Symmetric, so investigate the case NIZO. [V, MA, MI].

$$No=4.8V \Rightarrow Q_1=EOS$$
, and

$$VI = 4.8 + 0.7 + RS LB$$

= 5.5 + 10 × $\frac{1}{100}$ $\frac{4.8}{1}$

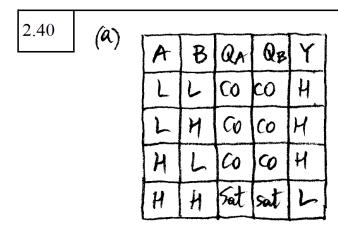
Eos

2.39 (D)

EOS

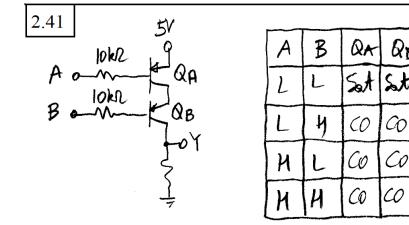
A	B	QR	QB	Y
L	2	CO	Co	H
L	H	Co	Sat	L
H	L	Sat	Co	L
H	H	Set	Sot	L

(b)
$$\beta_{\text{F(min)}} > (\frac{5-0.1}{1})/(\frac{5-0.8}{10}) \approx 12$$



(b)
$$\beta_{FA} \ge \left[\frac{5-2(0.1)}{1}\right] / \left[\frac{5-(0.8+0.1)}{10}\right] = 11.7$$

 $\beta_{FB} \ge \left[\frac{5-2(0.1)}{1} + \frac{5-(0.8+0.1)}{10}\right] / \left[\frac{5-0.8}{10}\right] = 11.$



2.42					
50	A	B	QA	QB	Y
Aom ar Born as	1	L	Sot	Sot	4
	2	Н	Sot	0	H
I kr 3	H	L	Co	Set	H
7	H	H	Co	Co	L

(a) Rz=(5-1.5-0.1)/10=0.34 W2 (use 330 S2).

ID= (5-1.5-0.1)/0.33=10.3MA

IB(min) = 10.3/50 = 0.206mA.

RIS (5-0.8)/0.206 = 20M

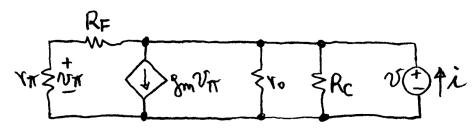
 R_1 R_2 R_3 R_4 R_4 R_5 R_4 R_5 R_4 R_5 R_5 R_4 R_5 R_5 R_5 R_6 R_6

KVL:
$$\sqrt{\pi} = -V$$
. kCL: $i + \frac{\sqrt{\pi}}{\sqrt{\pi}} + \frac{\sqrt{\pi} - \sqrt{v}}{\sqrt{v}} = 0$, or $i - \frac{V}{\sqrt{\pi}} - \frac{\sqrt{v} - \sqrt{v}}{\sqrt{v}} = 0$. Supernoode: $i = \frac{V}{\sqrt{\pi}} + \frac{\sqrt{c}}{\sqrt{c}}$, or $\sqrt{c} = R_C (i - \frac{V}{\sqrt{\pi}})$. Eliminating V_c gives

(b)
$$re = \frac{100}{101} \times \frac{26}{1} = 26\pi$$
, $r_0 = \frac{100}{1} = 100 \text{ kg}$
 $r_0 = \frac{100}{101} \times \frac{26}{1} = 26\pi$, $r_0 = \frac{100}{1} = 100 \text{ kg}$

1= V + V-Nc; V-Vc = 8mV+ Vc => V(PF-8m) = NC => NC = RF × (RC/No) 1-8m RF V = RC/(No) (1-fmRF) U; 1 = 0 + 1 [1 - REH(RE/1/2) (1-8mRF)]V = or [In + De RE+ (Retto) - Detto) + 8m Mx (Rc/No)] =N [+ + 1+ 8m (RC//16)] Ri = D = (+ 1+8m (Rcl/ro)) = 8T/ RF+(Rcl/ro) 1+1m/Rrl/ro) (b) VT= 100 (26/1)=2.6 hr, No= 100/1 = 100 hr, gm=1/(265) $Ri = 2.6 / \frac{10 + (1/100)}{1 + (1/100) \cdot 10^{3}/26} = 2.6 / 0.281 = 254 \text{ s.}$ (c) RF-70 and Rc-700 > BIT is diode-connected, and Ri= YAM/ [Hemy] > YAM = Ye = Z6.1. (d) R=>00 > Ri > VI/10=YT.

2.46 (a) 55M:

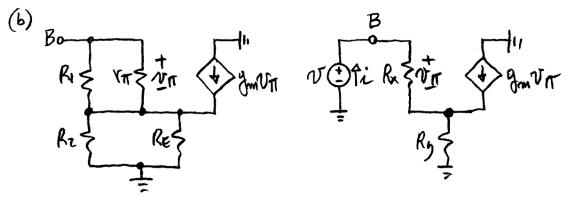


By inspection, Ro= RF/Ko//RC.

2.47 Apply test voltage
$$N$$
:

 $R_1 \ge \frac{R_2 V_{TT}}{R_1 + (R_2 V_{TT})} + V_{TT} = \frac{R_2 V_{TT}}{R_1 + (R_2 V_{TT})} + V_{TT} = \frac{N_1 + (R_2 V_{TT})}{R_1 + (R_2 V_{TT})} + V_{TT} = \frac{N_1 + (R$

2.48 (a) By inspection, $R_i = (R_1 + R_2)/(R_b)$. Using Eq. (53a), $R_i = (R_1 + R_2)/([X_T + (\beta_b + i)]R_E]$



With the switch closed, we get the circuit at the left. This, in turn, is equivalent to that at the right, provided we let $R_X = R_1 //V_T$ and $R_y = R_2 //R_E$. Applying a test voltage, as shown, we get, by KCL & KVL, $\frac{V_T}{R_X} + 9mV_T = \frac{N^2 - V_T}{R_Y}$. But, $V_T = R_X i$. Eliminating V_T , collecting, and taking the ratio $R_i = \frac{T}{i}$ gives $R_i = R_X + (1 + 9mR_X)R_Y$.

(c) $g_{m}=1/(262)$, $r_{m}=2.6kR$. For case (a) we get $Ri=(10+10)/(2.6+101\times10)=19.6kR$ ($2/R_1+R_2$). For case (b) we get $R_{x}=10//2.6=2.06kR$, $R_{y}=10//10=5kR$; $R_{i}=2.06+(1+\frac{3000}{26})5=969kL$ ($2/R_{i}+R_{i}+R_{i}$). This is much higher than (a)! The bootstrapping technique paises the input resistance dramatically!

(a) VE=(2/3)9=6V, Vc=(1/3)9=3V; RE=Rc=3/2= 1.5kl. Let Br=100. Then, IB=(2MA)/100 = 20 MA.
Improse PR=10IB=0.2 m A. ASSUMINX VEB(on)=0.7V, nve have VB=9-(6-0.7)=5.3V; R=(9-5.3)/0.2=18.5KR (use 18 km) and R2 = 5.3/(0.2+0.02) = 24 km. (b) RBB = 18/24=10.3 hR, VBB = 9×24/(18+24) = 5.14 V IC= VEE-VBB-VEB(on). Ic(morninal) = $\frac{9-5.14-0.7}{10.3/100+1.5} = 1.97$ mA $Tc(mox) = \frac{9-5.14(0.95)-0.7}{(10.3\times0.95)/150+1.5(0.95)} \approx 2.3 \text{ mA}$ $FC(min) = \frac{9-5.14(1.05)-0.7}{10.9\times1.05)/75+1.5/1.05} \approx 1.7mA$ (±0.3/2=±15% variation in Ic).

2.50

$$R_1 = \frac{2-0.7}{0.02} = 32.5 \text{ me } 33 \text{ kp}$$

$$I_{C} = \frac{5 - V_{C}}{R_{C}} - \left(I_{B} + \frac{0.7}{36}\right) = \frac{5 - 1.34 - 33I_{B}}{1.5} - I_{B} - \frac{0.7}{36}$$

1.97 mA, 2.17 mA. Not bad! Moreover, TCE=VC=

1.34+33Ic/B==2.44V, 1.99V, 1.90V, all near the

intended value of 2V.

(a) IB=3/150 = 20MA; DR = 40MA; R=0.7/0.04= 17.5 M (Use 18 M). TR= TRITTE= $R_2 = \frac{1}{20 \text{ MA}} \frac{13 \text{ MA}}{13 \text{ MA}} = 38.3 \text{ kg (wse 39 kg)}. \ P_R = I_C + \frac{1}{20 \text{ MA}} \frac{1}{20 \text{ MA}} = 38.3 \text{ kg (wse 39 kg)}. \ P_R = I_C + \frac{1}{20 \text{ MA}} = \frac{1}{20 \text{ MA}} \frac{1}{20 \text{ MA}} = \frac{1}{20 \text{ MA}$ FRZ= 3+0.06=3.06 MA; Rc= Rc \$ 13.06mA [-3-(-6)]/3.06=0.98 W (me 1 M). (b) $V_{C} = -0.7 - R_2 \left(I_B + \frac{0.7}{R_1} \right) = -0.7 - 39 \left(I_B + \frac{0.7}{18} \right) \Rightarrow$ VEC=0-VC=2.217+39 IB. IC=IRC-IR2, OL $I_{C} = \frac{6 - V_{EC}}{R_{d}} - (I_{B} + \frac{0.7}{R_{1}}) = \frac{6 - 2.217 - 39I_{B}}{1} - I_{B} - \frac{0.7}{10}, or$ IC=3.74-40IB=3.74-40 IC=3.74/(1+40). $IC(min) = \frac{3.74}{1+40/75} = 2.44 \text{ m/A}^{\circ}, Ic(mom) = \frac{3.74}{1+40/150} = 2.96$ MA; I((max)= 3.74 = 3.73 m.A. Correspondingly) VEC (max)=2.217+39(2.44/75)=3.49 V; VEC(mom)= 2.99 V, VEC(min) = 2.77 V.

2.52 (a) $I_{C2} = I_{C1} = (5-0.7)/4.3 = 1.0 \text{ mA}$

(b) Icz=Ic1exp(DVBE/VT)=1.0exp(2/26)=1.080 mA

(c) ICZ= IC1 exp (2x5/26) = 1.469 mA

(d) VBE1 = 100 - 2×10 = 680 mV;

IC1=(5-068)/4.3=(4.32/4.3) mA;

 $I_{C2} = \frac{4.37}{4.3} \exp(-2 \times 10/26) = 0.466 \text{ mA},$

(e) Now we must have $T(Q_1) > T(Q_2)$, such that

 $T(Q_1)-T(Q_2)=\frac{26}{2}\ln\frac{1.0}{0.75}=3.74$ °C.

 $I_{G} = (5-0.7)/4.3 = 1.0 \text{ m/s}$

(a) ICZ=0.4mA= (1mA/10) × 2×2. By the rule of thumb, VBtZ=700-60 H8H8=700-24mV > DVR=24mV;

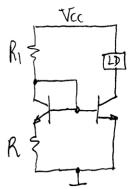
R= AVR/IR= 24/0.4=60 JZ

(b) DVR = 60+18=78 mV; R=78/0.05=1560 sc.

(C) DVR = (26mV) In (1000/173) = 54.5mV, R=54.5/0.123 = 443 s.

(a) $V_{BEI} = (26 \text{ mV}) \ln \frac{(6-0.7)/104}{2 \times 10^{-15}} \approx 684 \text{ mV}$ VBEZ=0.026 ln 0.184-VBEZ; start outwith VBEZ=0.6V. TBEZ = 0.026 M 0.684-0.6 = 0.636 V $\sqrt{8E2} = 0.026 \text{ ln} \frac{0.684 - 0.636}{2 \times 10^{-12}} = 0.620 \text{ V}$ Iterate further, and end with VBEZ = 626 mV. Icz=(0.684-0.676)/103~ 58MA. (c) With Vcc = 6V, Ic1 = (6-0.684)/10=0.5316; (1/2)Ic1=0.5316/2=0.2658; Rule of Thumb: VBEI = 684-18=0.666 V; Vcc=0.666+10×0.2658= 3.324 V. Reiterate as before, and find VBEZ=0.026 ln 0.666-VBEZ => VBEZ=620mV=> Icr=(0.666-0.620)/103=46 MA. While Ici has droped to & its initial value, For has droped from 58 MA to 46 MA. Not 1/2 per Icz is not linearly proportional to Ic1.

2.55



(a) Is=2fA=> VBE=700 mV@ Ic=1mA.

 $I_{C1}=0.5_{MA} \Rightarrow V_{BE1}=700-18=682_{mV}$ $I_{C2}=7_{mA} \Rightarrow V_{BE2}=700+18=718_{mV}$ $I_{C2}=7_{MA}=7_{MA}$

RI= (5-0.718)/0.5=8.564 hr.

(b) IC1 = 1mA => VBE7 = 700mV; VR=72×1=72mV. VBEZ= 700+72=772mV=(700+4×18)mV=IC2=1×24= 16mA. Thus, while Ic1 has doubled once, Ic2 has doubled four times!

(a) $R_1 = (12 - 5.6)/3 = 2.1 \text{ kg (me 2.0 kg)}.$

Rz = (5.6-0.7)/2 = 2.45 km (me 2.4 km).

gm= 2/26=1/(1312); Ym=100x13=1.3hl; Yo= 75 = 37 kl2. Rc=Yo[1+gm(R2//Ym)]=37[1+(2400//1300)/13]=2.5 M.S.

(b) An increase in V_L decreases VCE and thus decreases Io. The change is such that $\Delta I_0/\Delta V_L = -\frac{1}{Rc} = -\frac{1}{2.5 \times 10^L} = -0.4 \text{ MA/V}$. An increase in $|\Delta V_{EE}|$ in creases both V_{-} and V_{0E} according to

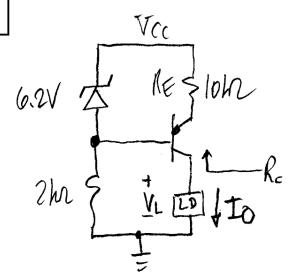
Vz and Vce, according to

ΔVZ = \(\frac{\gamma_{\mathbb{E}}}{R_1+\gamma_{\mathbb{E}}} | \Delta \VEE | = \frac{15}{2000+15} | \Delta \VEE | = \frac{|\Delta \Vee}{134}, \Delta \Vee | \lefta \Vee |.

DIO= AVZ + AVCE = 134×24×103 + (AVEE) = (3.1+0.4)106 | AVEE |.

: 0 ATO = 3.5 MA/V.

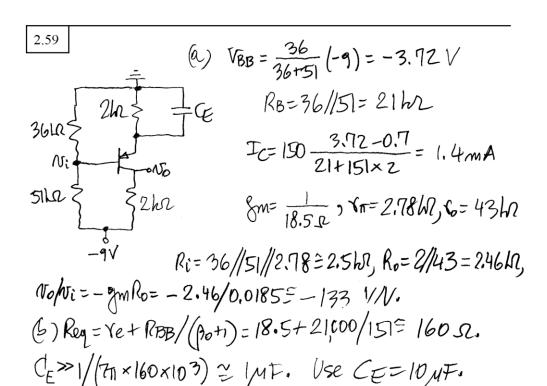




An increase in Vi decreases Vec and thus decreases To.

An increase in Voc increases Vz as well as VEC

(a) $I_B = \frac{10-0.7}{32+151\times8.2} = 7.32 \text{ MA}; I_{t=1.097 \text{ mA}};$ VB= 33 × 7.32×10-3 = 0.241 V VE = VB + VEB(M) = 0.241+0.7 = 0.941 V $V_r = -10 + 4.7 \times 1.097 = -4.842 V$. $g_{m} = \frac{1.097}{76} = \frac{1}{23.7\pi}$; $f_{0} = 3.55 M$; $f_{0} = 45.5 M$. Ri= 33//3.55 = 3.2W; Ro=4.7//45.5 = 4.26W. $\frac{v_0}{v_{sig}} = \frac{3.2}{0.3+3.2} \left(-\frac{4260}{23.7} \right) \frac{12}{4.76+12} = -121 \text{ V/V}.$ (b) VB=VB+Vb=0.241V+3.2 (5mV) coswt = 0.241 V + (4.57 mV) conwt; Vd=Vc+Vc=-4.842V-121 (5mV) coswt; = -4.842V + (0.605 V) cos (wt -180°); No = 0+ (0.605V) con (wt-180°); NE=0,941V+0.



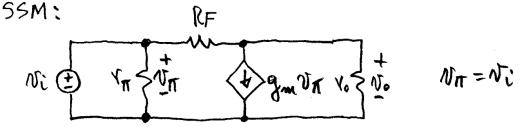
[V, MA, ka], kNL: 10=3.9 IE+68 IE/121+0.7 >

IE=2.08 mA > IC=2.07 mA > gm=1/(12.6 D), VIT =

1.5 LR, Vo = 48 LD, Rc//Vo = 3.9/48 = 3.6 LD

$$R_i = VIT / \frac{R_F + (Rc/N_0)}{1+8m(Rc//V_0)} = 1.5 / \frac{68+3.6}{1+3600/12.6} \approx 214 D$$
 $R_i = VIT / \frac{R_F + (Rc/N_0)}{1+8m(Rc//V_0)} = 3600 / [12.6 + \frac{68000}{121}] = 495 D$
 $V_i = \frac{V_0}{R_F} = \frac{V_0}{N_0} V_i = \frac{V_0}{R_F} \frac{V_0}{R_F} = \frac{V_0}{R_F} \frac{V_0}{N_0} = -(\frac{1}{12.6} - \frac{1}{68000}) (6800 / 3600) = -271 V/V.$

2.61 (a) IE=IBIAS = 1 mA; IC= OFIE = 0.99 mA; IB= IE/(BF+1)=(1/101) mA; VC = VBE+RFIB = 0.7+100/101 = 1.7 V. Vo = 100/0.99 = 101 kN; 8m= 0.99/26=1/(26.3 sq).



KCL: $\frac{v_i - v_o}{RB} = g_m v_i + \frac{v_o}{v_o}$; $v_i (\frac{1}{RB} - g_m) = \frac{v_o}{RF} + \frac{v_o}{v_o} = \frac{v_o}{R_F / R_o}$; $\frac{v_o}{v_i} = -g_m (R_F / R_o) (1 - \frac{1}{g_m R_F}) = -\frac{0.99}{26} (100 / 101) 10^3 (1 - \frac{1}{105 / 26.3})$ = -1913 V/V.

(b) gm doubles to $2\times0.99/26$, and 70 halves to 50.5 kR. From (a), it is apparent that $10/10i \cong -9m$ (RF/170), so $\frac{10.98}{10} = -\frac{1.98}{26} (100/150.5) 10^3 = -2555$ V/V. Because of the presence of RF, which remains unchanged, the doubling of 9m prevails over the habring of 9m prevails over the habring of 9m, so the gain magnitude increases.

MCL:
$$\lambda_i = \frac{V_i + V_i - V_o}{R_F} = \frac{V_i}{K_R} - \frac{V_o}{R_F}$$
 $\frac{V_i - V_o}{R_F} = \frac{V_i}{K_R} - \frac{V_o}{R_F}$
 $\frac{1 - 8mR_F}{R_F} V_i = \frac{V_o}{R_F} = \frac{V_o}{R_F}$

$$N_{0} = \frac{1-q_{m}R_{F}}{R_{F}+Y_{0}}N_{i} = \frac{1-q_{m}R_{F}}{1+R_{F}/Y_{0}}N_{i} \Rightarrow i_{i} = \frac{N_{i}}{Y_{F}/R_{F}} - \frac{1-q_{m}R_{F}}{R_{F}(1+R_{F}/Y_{0})}N_{i}$$

$$R_{i} = \frac{N_{i}}{N_{i}} = \frac{N_{i}}{N_{i}} = \frac{N_{i}}{N_{F}} - \frac{1-q_{m}R_{F}}{R_{F}(1+R_{F}/Y_{0})} = 2.6/100/\frac{100(1+100/100)}{100/0.026-1} = 52.52.$$

If $R_1=1001$, replace (o with $100/R_1=100/100=50 M$. Then, $R_i=2.6/(100)/\frac{100(1+100/50)}{100/0.026-1}\cong 76 \Omega$. Ri is dominated by the third term, roughly representing R_F divided by the gain $|V_0/V_i|$ (Miller effect). Loading the amplifier reduces the gain and thus increases R_i .

With Rsig ≠0, NT ≠0 and gm NT ≠0, so is increases, reducing Ro. In the limit Rsig >00, we get Ro > 1 br.

[V, mA, kn]: DC analysis;

$$I_B = \frac{10-0.7}{33+176\times8.2} = 8.72 \text{ mA}$$
 $8.2 \le 270 \text{ n}$
 $I_C = 125\times8.72 = 1.09 \text{ mA}$
 $g_m = \frac{1.09}{26} = \frac{1}{23.8 \text{ n}}$
 $g_m = \frac{1.09}{26} = 23.8 \text{ n}$
 $g_m = 125\times23.8 = 2.98 \text{ M}$
 $g_m = 125\times23.8 = 2.98 \text{ M}$

$$Ri = RB//Rb = 33//[2.98 + (125 + 1)(8.21/0.22)] = 15.9 \text{ KZ}$$

$$R_0 \approx 8.2 \text{ k/L}$$

$$\frac{N_0}{N_{\text{sij}}} = \frac{15.9}{0.3 + 15.9} \left(-\frac{1/23.8}{1 + (1/23.8)(8200/1200)} 8200 \right) \frac{12}{8.2 + 12}$$

$$= -17.2 \text{ V/V}$$

[2.64] (a)
$$T_{c}=125 \frac{12-0.7}{100+126\times15}=0.71 \text{ mA}$$
; $g_{m}=0.71/26\cong 1/(37 \Omega)$; $T_{m}=125\times37\cong4.6 \text{ k}\Omega$.
 $Ri=(100 \text{ k}\Omega)//(Rb=100)/([4.6+126(15//0.1)]=14.6 \text{ k}\Omega$; $R_{o}=10 \text{ k}\Omega$.
 $\frac{N_{o}}{N_{i}}=-\frac{g_{m}}{1+g_{m}(15//0.1)}\frac{1}{10^{3}}R_{o}=-\frac{10,000/37}{1+99.3/37}=-74 \text{ V/V}$.
(b) $Reg=100\Omega+15 \text{ k}\Omega//(Re=100)+[15,000)/(37+\frac{10^{5}}{176})$

Use 20 mt. (c) Without C, the gain drops to $\frac{v_0}{v_1} = \frac{10 \text{ M}}{15 \text{ km}} = -0.67 \text{ V/V}.$

= 887s. C> 1/(6.78×887×100) = 1.8 MF.

[2.65] (a) RBB = 30//15 = 10 kR, VBB = [15/(30+15)]9 = 3V. $Ic = 100 \frac{3-0.7}{10+101\times2.2} = 0.99 \text{ m/k}$; $8m = \frac{1}{76\pi}$; VT = 7.6 kR. $Ri = 10/[7.6+101\times0.2] \approx 7 kR$; $Ro \approx 2.7 kR$ $\frac{N_0}{V_i} = -\frac{1/26}{1+200/26} 2700 = -11.9 V/V$ (b) $Reg = \frac{2}{1000}/[200+26+\frac{10,000}{101}] \approx 280 \Omega$ (c) $\frac{N_0}{N_i} \approx -\frac{2.7}{2+0.2} = -1.2 V/V$, quite low!

2.66
$$V_{c}$$
 V_{i}
 V_{i}

 $\begin{array}{l} 2.67 \\ \text{(a) } Ri = \text{Ym} + \left(\frac{1}{1} \right) \left(\frac{1}{1$

where we are assuming
$$r_0 >> R_L$$
.
 $0.853 = \frac{1}{1 + \frac{0 + 977}{(\beta_0 + 1)300}} = \frac{1}{1 + \frac{7e}{300}} \Rightarrow r_0 = 51.7.52$

> Ic= 7/1e=26/51.7=0.5 mA.

$$0.718 = \frac{1}{1 + \frac{Rasg + rir}{(30+1)RL}} = \frac{1}{1 + \frac{10^4}{(30+1)300} + \frac{re}{300}} = \frac{1}{1 + \frac{33.3}{300} + \frac{51.7}{300}}$$

$$\frac{N_0}{N_{\text{Sig}}} = \frac{150 \text{ ; } N_{\text{T}} = 151 \times 51.7 = 7.75 \text{ km.}}{1 + \frac{29000 + 7.755}{151 \times 1200}} = 0.867 \text{ V/V.}$$

 $\begin{array}{ll}
\overline{V_{BB}} = \frac{68}{68 + 47} (-12) = -7.1 \text{ V}, R_{BB} = 68 / 47 = 27.8 \text{ bl.}, \\
\overline{V_{C}} = 125 \frac{7.1 - 0.7}{27.8 + 126 \times 3} = 1.97 \text{ m/s}, & e = \frac{26}{1.97} = 13.2 \text{ sl.}, & \text{m} = 125 \times 13.2 = 1.65 \text{ bl.}, & \text{s} = 80 / 1.97 = 40.6 \text{ m} = 41 \text{ bl.} \\
R_1 = R_{BB} / \left[\frac{1}{100} + \frac{1}{100} (R_{B} / R_{BB}) - \frac{27.8}{100} \right] = 27.8 / \left[\frac{1.65 + 126}{1.65 + 126} (3 / 2 / 41) = 23.4 \text{ bl.} \\
R_0 = R_{E} / \frac{1}{100} \left[\frac{1}{100} + \frac{1}{100} \frac{1}{100} \right] = 3 / 4 / \left[\frac{1}{100} \frac{1}{100} \right] = 20.7 \text{ sl.} \\
\frac{23.4}{1+23.4} \sqrt{100} = \frac{1}{100} \frac{1}{100} = 0.959 = 0.959 = 0.959 = 0.959 \\
\frac{1}{100} = 0.959 \frac{1}{1200} = 0.959 = 0.959 = 0.959 = 0.942 \text{ V/V}.
\end{array}$

2.70 (a)
$$T_{c}=100 \frac{6-0.7}{20+101\times3}=1.64mA$$
, $4e=15.7 \Omega$, $1000 = 1.64mA$, $10000 = 1.64mA$, 10000

$$\frac{\frac{100}{3}\text{Vsig}}{\frac{1}{3}\text{Vsig}} = \frac{1}{1 + \frac{1.6 + (10/120)}{101 \times 3}}$$

$$\frac{N_0}{N_{\text{vs}}} = 0.649 \text{ V/V}$$

(b) With Cz in place, the upper 10-br resistance is placed in parallel with $r_{\rm F}$, giving $r_{\rm H}(e_{\rm F}) = 10//1.6$ $\cong 1.4 \, \rm kr$; the lower 10-kr resistance is placed in parallel with RE, giving $r_{\rm E}(e_{\rm F}) = 10//3 = 2.3 \, \rm kr$. We now have

 $R_{0} = \frac{10000}{R_{0}} + \frac{1000}{R_{0}} + \frac{1000}{R_{0}} = 1.4 + 101 \times 2.3 = 234 \text{ hz}$ $R_{0} = \frac{10000}{R_{0}} + \frac{10000}{R_{0}} = \frac{1000}{R_{0}} + \frac{10000}{R_{0}} = 11052$

Bootstrapping micreases hi significantly, thus reducing injust loading and making gain closer to unity.

Resolution Ve REIN -12V

Impose $I_0=1$ MA, $V_{Cl}=6V$. $\Rightarrow R_C=6$ We (we 6.2 k Ω , 5%) We know that 0 = 1V/V, so to achieve 0 = 1V/V we need $R_{El}=R_C=6.2$ W. Also, to ensure $I_C=1$ MA, we need $R_{El}+R_{El}=(12-0.7)/1$, or $R_{El}=11.3-6.2=5.1$ k Ω , 5%.

Reg = RE2//(RE1+Ve) = 5.1//(6.2+0.026) = 2.8 kR. $C > \frac{1}{2\pi \times 2.8 \times 10^3 \times 10^4} = 5.7 mF$. Use $C = 0.1 \mu F$.

$$T_{C} = \frac{12 - 0.7}{15} = 0.753 \text{ m/t}$$

$$Y_{e} = \frac{26}{0.753} \approx 35 \Omega. \quad R_{o} \approx 10 \text{ h/z}.$$

$$R_{i} = 35 // (15 \text{ h/t}) \approx 35 \Omega.$$

$$V_{e} = \frac{0.035}{0.035 + 0.1} N_{sig} = 0.26 N_{sig}.$$

No= 9m Ve Ro = 1 (0.26 Nsig) 10,000 = 74 Nsig. No/Nsig = 74 V/V.

Full Download: http://testbanklive.com/download/analog-circuit-design-discrete-and-integrated-1st-edition-franco-solutions-manu