CHAPTER 2

PROBLEM #2-1 1, 1,4 D = 1,4 (100) = ------ 140 PSF 2.1.2D + 1.6L + 0.5 (Lr or Sor R) 1.2 (100) + 1.6 (70) + 0.5 (30) = ---\_\_\_\_\_ 247 PSF 3. 1.20 + 1.6 (Ly or 5 or R) + (0.56 or 0.5W) 1.2 (100) + 1.6 (30) + 0.5 (70) = \_\_\_\_\_ 203 psF 4. 1.20+ 1.0 W + 0.5L + 0.5 (Ln or 5 or R) Download: http://alibabadownload.com/product/structural-steel-design-5th-edition-mccormac-solutions-manual 1,2(100) + 1,0(0) + 0.5(70) + 0,5(30) = \_\_\_\_\_ 170 PSF 5. 1.2D + 10E + 0.5L + 0.25 6. 0,9 D+ 1,0 W 90 PSF 7. 0.9 D + 1.0E 2-1

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1, 1,40 = 1,4 (12000) = --16,80016 2. \_\_\_\_ DOES NOT CONTROL (BY INSDECTION) 3. 1.20 + 1.6 (Lr or Sor R) + (0.5L or 0.5W)  $1.2(12,000) + 1.6(\phi) + 0.5(+52,000) = -$ -40,400/b 4. 1.20 + 1.0W + 0.5L + 0.5/L+ OR S or R) 1.2 (12,000)+ 1.0/52,000) = -66,4001b « DOES NOT CONTROL 5. (BY INSPECTION) 0,9(0) + 1,0 W (UPLIFT) 6. -41,200/be 0.9(12000) + 1.0(-52,000) = 7. DOES NOT CONTROL (BY INSPECTION)

MAXIMUM FACTORED LOADS: + 66,400 16 CASE 4. - 41,200 16 CASE 6.

2-2

- 4. 1120 + 1.0W + 0.5L + 0.5 (Lrorsor R) 112 (9000) + 1.0 (\$) + 0.5 (5000) + 0.5 (2500) = --- 14,550 /b
- 5. 1.2D + 1.0 = + 0.5L + 0.25 $1.2(9000) + 1.0(6500) + 0.5(5000) + 0.2(\phi) = - 19,800/b$
- 7. D.9D + 1.0E (UPLIFT) 0.9(9000) + 1.0(-6500) = \_\_\_\_\_\_ 1,600 lb

MAXIMUM FACTORED LOADS: + 20,050 16 CASE 2 NO UPLIFT

SFCV

2-4-

D=20PSF 5=12PSF, LY=18PSF, W= 38PSF 1 (-) 16PSF + (+) BEAM SPACING = 6-0" D (PLF) = 20(6) = 120 PLF 5 (PLF) = 12(6) = 72 PLF Lr (PLF) = 18(6) = 108 PLF W (PLF) = -38(6) = -228 PLF OR = +16(6)= 96 PLF 1.40 = 1.4/120) = ----1. 168 PLF 2. 1.2 D + 1.66 + 0.5/6+ or Sor R) 1.2 (120) + 0.5 (108) = ----198 PLF 3. 1120 + 1.6 (LrorSorR) + (0.5L or 0.5W) 1.2(120) + 1.6 (108) + 0.5 (96) = \_\_\_\_\_ 364.8 PLF 4. 1.20 + 1.0W + 0.5L + 0.5 (Lror Sor R) 1.2 (120) + 1.0 (96) + 0.5/108) = \_\_\_\_\_ 294 PLF 5. 1.20 + 1.0E + 0.5L + 0.25 1,2(120) + 0.2(72) = \_\_\_\_ 158.4 PLF 6. 0.90 + 1.0 W (UPLIFT) 0.9 (120) + 1.0 (-228) = -120,0 PLF --- DOES NOT CONTROL - BY INSPECTION 7. MAXIMUM FACTORED LOADS: 364.8 PLF CASE 3, DOWNWARD -120,0 PLF CASE G. UPWARD

\_\_\_\_\_ 100 PSF D 1. Z 100 = 2. D'+L = 100 + 70 = ------ 170 PSF 3. D + (Lrorsor R) = 100 + 30 = ----- 130 PSF 4. D+ 0.75(L)+ 0.75(Lr or SorR) 100 + 0.75 (70) + 0.75 (30) = \_\_\_\_ 175 psF 4 5. D + (0.6 Wor 0.7 E) = 100 +0 \_\_\_\_\_ 100 psF 6a. D+ 0.75 L + 0.75 (0.6W) + 0.75 (4 or Sor R) 100 + 0.75 (70) + 0 + 0.75 (30) ----- 175 PSF 6b. D+ 0.75L + 0.75 (0.7 E) + 0.75 (s) 100 + 0.75 (70) + 0 + 0.75 (30) \_\_\_\_\_ 175 psF 7 0.6 D+ 0.6W (UPLIFT) 0.6 (100) + 0 \_\_\_\_\_ - 60 PSF (NO 0.6D + 0.7E (UPLIET) B 0.6(100)+0 \_\_\_\_\_ GOPSE (NO UPLIET)

GOVERNING LOAD = 175 PSF CASE 4.

12,000 16 1. D = 12000 - 12,000 16 2, D+L = 12,000 = -\_\_\_\_ 12,000/b 3. D+ (Lror Sor R) = 12,000 = 4. D + 0.75 L + 0.75 (Lror SorR) 12,000 16 12,000 = 5. D+ (0.6Wor0.7E) - 43,200 lb 4 12,000 + 0.6 (52,000)=\_\_\_\_ 6a. D + 0.75L + 0.75 (0.6W) + 0.75 (Lr or Sor R) 12,000 + 0 + 0.75(0.6)52,000 + 0 = - 35,400 lb 66. D+ 0.75L + 0.75 (0.7E) + 0.75 (5) 12,000 +0 = 12,000 /b 0.6D + 0.6W (UPLIFT) 7. 0,6(12,000) + 0,6(-52,000) = -----24,000 lb (UPLIFT) 8. 0.60 + 0.7E 0.6 (12,000)+0= -7,200 /b (NOUPLIFT) GOVERNING LOADS: + 43,200 16 CASE 5. - 24,000 16 CASE 7.

2-8

PROBLEM # 2-9

1. D = 9000 =	- 9,000/b
2. D+L = 9000 + 5000 =	14,00016
3. D + (Lr or 5 or R) = 9000 + 2500 =	11,50016
4. D+ 0.75 L + 0.75 (L+ or 5 or R)	
9000 + 0.75 (5000) + 0.75 (2500) =	14,625/6
5. D+ (0.6Wor0.7E)	
9000 + 0.7 (6500) =	13,5501b
6a. D+ 0.75L+ 0.75 (0.6W)+ 0.75 (Lr or Sor R	)
9000 + 0.75 (5000) + 0 + 0.75 (2500)=	)= 18,037.5 /b -
7. 0.6 D + 0.6W UPLIFT	
0.6(4000)+0=	5,400 lb (No UPLIFT)
8. 0,60 + 0,7 E UPLIFT	OPLIFT
0.6 (9000) + 0.7 (-6500) =	850 lb (NO OPLIFT)
GOVERNING LOADS:	OPLIFT)
G LOADS:	
18,037,5 16 CASE 60.	
NO UPLIET	

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1. D = 24 = 24P5F 2. D+L = 24 = . 24 PSF 3. D+ (Lror Sor R) = 24+16 = 40 PSF 4. D+ 0.75L+ 0.75 (Lror Sor R) 24 + 0.75(16) = -36 PSF 5. D + (0.6W or 0.7E) 24 + 0.6 (42) = \_\_\_\_\_ 49.2 PSF 6a. D + 0.75 L + 0.75 (0.6W) + 0.75 (Lr or Sor R) 24+0+0.75(0.6)(42)+0.75(16)= 54.9 PSF 66. D+ 0.75L + 0.75 (0.7E) + 0.75 (L+ or 5 or R) 24 +0 + 0 + 0.75 (16) = \_\_\_\_\_ 36 PSF 7. 0.60 + 0.6 W UPLIFT 0.6 (24) + 0.6 (-42) = ----10.8 psF -UPLIET 8. 0.60 + 0.7E UPLIFT 0.6 (24) +0 = \_\_\_ 14,4 PSF (NO UPLIFT) GOVERNING LOADS: 54.9 pSF CASE Ga. -10.8 PSF CASE 7, UPLIFT

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2-10

PROBLEM # 2-11	
D=64psF L=100psF	
BEAM SPACING = 76"	
D (PLF) = 64(7.5) = 480 PLF	
L (PLP) = 100 (7.5) = 750 PLF	
1. 0 = 480 =	480 PLF
2, D+L = 480+750 =	
3. D + (Lror 5 or R) = 480 =	
4. D+ 0.75L + 0.75 (Lrorsor R) 480 + 0.75 (750) =	10,10
	1042,5 PLF
5. D + (0.6W or 0.7E) = 480 =	480 PLF
6a. D + 0.75L + 0.75 (0.6W) + 0.75 (L+ 0+	Sor R)
480 + 0.75 (750) =	- 1042,5 PLF
66. D + 0.75L + 0.75 (0.7E) + 0.75 (Lyor 480+ 0.75 (75) =	
480 + 0.75 (750) =	
7. 0.60 + 0.6W UPLIFT	- 104215 PLF
0.6 (480) +0 =	- 288.puF
8. 0.60 + 0.7E	200 ptf
0.6 (4.80) +0=	200 - =
	288 PLF
GOVERNING LOAD:	
SFCV 1230 PLF CASE 2.	

 $D = 20 \text{ psf} \qquad S = 12 \text{ psf}, \ L_r = 18 \text{ psf}, \ W = 38 \text{ psf} \uparrow (-)$   $BEAM SPACING = 6'-0^{n} \qquad 16 \text{ Psf} \downarrow (+)$  D (PLF) = 20 (C) = 120 PLF S (PLF) = 12 (C) = 72 PLF  $L_r (PLF) = 18 (C) = 728 \text{ PLF}$  N (PLF) = -38 (C) = -228 PLF + 16 (C) = 96 PLF

1. D = 120 = 120 PLF 2. D+L = 120 = \_\_\_\_ 120 PLF 3. D + (Lr or 5 or R) = 120 + 108 = ----228 PLF 4. D + 0.75L + 0.75 (Lror Sor R) 120 + 0,75 (108) = \_\_\_\_ ZOI PLF

5. D + (0.6WOrD.7E) 120 + 0.6 (96)= \_\_\_\_ 177.6 PLF

6a. D+ 0.75L + 0.75 (0.6W) + 0.75 (LrorSorR)

120 + 0 + 0.75 (0.6) (96) + 0.75 (108)= 244.2 PLF = 66. D + 0.75L + 0.75 (0.7E) + 0.75 (Lr or 5 or R)

120+0+0+0.75(108)= \_\_\_\_\_ 201PLF 7. 0.60+0.6W UP4FT

0.6 (120) + 0.6 (-228) = -64.8*PLF* UPLIFT GOVERNING LOADS: 244.2 PLF CASE GA. - 64,8 PLF CASE 7. UPLIFT 8.